

## Sensorless Code-Free FOC BLDC Motor Controller

### FEATURES AND BENEFITS

- 40 V maximum rating with integrated buck regulator for high efficiency
- Fully integrated single-shunt sensorless FOC controller (code-free)
- Speed, torque, and power mode operation
- Power-loss brake functionality
- Universal speed curve
- Fault mode brake
- Analog/PWM/Clock mode speed control
- Precision speed control
- Configurable RD or FG output
- Slew-rate control for electromagnetic-interference (EMI) mitigation
- Proprietary nonreverse fast startup
- Ultra-quiet low-speed operation
- Current-control soft start
- Windmill startup operation
- No  $V_{BB}$  boost on powerup with spinning motor
- I<sup>2</sup>C serial port
- Power limit protection
- Configurable current and power limit
- Lock detection
- Overcurrent limit (OCL)
- Overvoltage protection (OVP)
- Short-circuit protection (OCP)
- Logic input compatible with 3.3 V and 5 V

### DESCRIPTION

The A89333-1 is a three-phase, sensorless, brushless DC (BLDC) motor controller. A field-oriented control (FOC) algorithm is fully integrated to achieve the best efficiency and acoustic noise performance. The device also optimizes motor-startup performance in stationary, forward, and reverse windmill conditions.

Programmable profiles and closed-loop controls are included for constant power and constant speed operations. This eliminates the requirement for a microprocessor-based system and minimizes programming requirements.

A simple inter-integrated circuit (I<sup>2</sup>C) interface is provided for setting motor-related parameters, control-related parameters, and startup profiles, which are stored in nonvolatile memory (NVM). The I<sup>2</sup>C interface can also be used to control the motor directly and to provide speed and status feedback. Password protection is available for stored NVM data.

The A89333-1 is available in a 28-contact 4 mm × 4 mm quad-flat no-leads (QFN) package with exposed thermal pad (suffix EC).

### APPLICATIONS

- Server fans
- Telecommunications (telecom) fans
- Home appliance fans

### PACKAGE

28-Contact QFN with exposed pad (EC package)

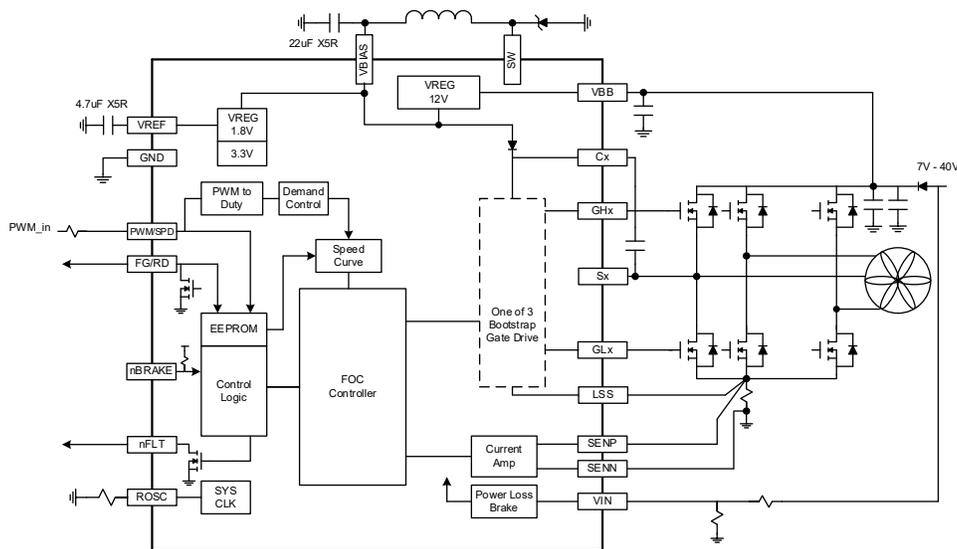
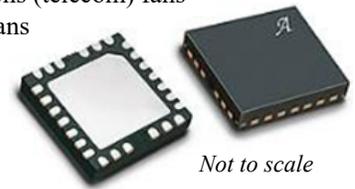


Figure 1: Typical Application with Buck Regulator



## TABLE OF CONTENTS

Specifications .....	4	Diagnostic and Protection Features .....	22
Pinout Diagram and Terminal List Table .....	5	VBB Undervoltage—VBB UVS .....	22
Pin Descriptions.....	9	VBB, UV, and NVM Reprogramming .....	22
VBB .....	9	Overtemperature Protection—OVT/TSD .....	22
VIN.....	9	Overcurrent Protection—OCP (Short Protection) .....	23
VREF .....	9	Loss of Sync (Lock/Stall Detection).....	23
VBIAS .....	9	No-Motor Start .....	24
SW .....	9	VBB Overvoltage Variable Limiter .....	24
FG/RD .....	9	Overcurrent Limit .....	24
PWM/SPD .....	9	Maximum Power Limit .....	24
ROSC .....	9	Application Features.....	25
Sx .....	9	EEPROM NVM for Storing Motor Control and Configuration Data .....	25
Cx .....	9	FG/RD Pin .....	25
GHx .....	9	FG .....	25
GLx .....	9	RD.....	26
LSS.....	9	FG in VBB UV Condition.....	26
SENN.....	9	FG ID Pattern Generation.....	26
SENP .....	9	Dead Time Configuration .....	27
nBRAKE .....	10	Slew Rate Control.....	27
nFLT.....	10	Buck Converter.....	27
Functional Description .....	11	Advanced Features .....	28
Powerup and Initialization.....	11	BEMF Compensation.....	28
External Command Source .....	12	Soft-Off Deceleration .....	28
Analog Input Voltage (EXT_CMD_SRC, 0x1). .....	12	Soft Start.....	28
Frequency Mode (EXT_CMD_SRC, 0x3).....	13	Quiet Start.....	28
I <sup>2</sup> C Mode (EXT_CMD_SRC, 0x0).....	13	Forced OL.....	28
Universal Curve Controller: UCC.....	14	VIN and Power-Loss Brake .....	29
Motor Rotation Direction.....	15	No-Power Brake .....	30
Speed, Torque, or Power Control Modes.....	16	Registers and Nonvolatile Memory (NVM) Map .....	31
Speed Mode (0x0).....	16	User Registers.....	41
Torque Mode (0x2).....	16	SW Status Register, SW_STATUS .....	42
Power Mode (0x1) .....	16	I <sup>2</sup> C Command Register, REF_CMD.....	43
Maximum System Speed.....	16	SW Fixed-Address Variables .....	44
Maximum System Current and Bus Current Sensing.....	16	FOC Internal Variables .....	45
DC-Link Voltage.....	17	Programming the EEPROM .....	46
Maximum Electrical Power .....	17	I <sup>2</sup> C Serial Interface .....	46
Speed Limit.....	17	I <sup>2</sup> C Timing Diagrams.....	46
Power Limit.....	17	Read Procedure.....	46
Current Limit .....	17	Write Procedure.....	47
Motor Control Application (MCA) Finite State Machine (FSM) .....	17	Operation Modes and Customer Password Protection .....	48
Standby—SBY .....	18	Application Information.....	49
Windmilling—WMDML .....	18	Layout Notes.....	50
IPD and Align .....	19	Pin Diagram.....	51
Ramp-Up—RAMPUP .....	19	Package Outline Drawing .....	52
Drive—DRIVE.....	20		
Regenerative Mode .....	20		
Brake—BRAKE.....	20		
FOC Algorithm Speed and Current Loop.....	20		
Observer.....	21		

## SPECIFICATIONS

### SELECTION GUIDE

Part Number	Package	Packing
A89333GECRSR-1	28-lead 4 mm × 4 mm QFN with exposed thermal pad	6000 pieces per 13-inch reel



### ABSOLUTE MAXIMUM RATINGS [1][2]

Parameter	Symbol	Conditions	Rating	Units
Supply Voltage	$V_{BB}$	$V_{BB} = 40\text{ V}$	-0.3 to 40	V
Power Loss Brake Terminal	$V_I$	$V_{IN}$	-0.3 to 40	V
Speed Control Terminal	$V_I$	PWM/SPD	-0.3 to 40	V
Logic Input Terminal	$V_I$	nBRAKE	-0.3 to 6	V
Logic Bidirectional Terminal	$V_{IO}$	FG/RD	-0.3 to 40	V
Logic Output Terminal	$V_O$	nFLT	-0.3 to 6	V
Buck Switch Terminal	$V_{SW}$		-1 to 40	V
		$t_W < 0.5\ \mu\text{s}$	-4 to 40	V
Bootstrap Supply Terminals	$V_{CX}$	CA, CB, CC	-0.3 to $V_{BIAS} + 40$	V
Motor-Phase Terminals	$V_{SX}$	SA, SB, SC	$V_{CX} - 4$ to $V_{CX} + 0.3$	V
High-Side Gate Drive Output Terminals	$V_{GHX}$	GHA, GHB, GHC	$V_{SX} - 0.3$ to $V_{CX} + 0.3$	V
Low-Side Gate Drive Output Terminals	$V_{GLX}$	GLA, GLB, GLC	$V_{LSS} - 0.3$ to $V_{BIAS} + 0.3$	V
Input Terminal	$V_I$	ROSC	-0.3 to 6	V
Output Terminal	$V_o$	VBIAS	-0.3 to 15	V
Output Terminal	$V_O$	VREF	-0.3 to 3.4	V
Input Terminal	$V_I$	SENP, SENN	-4 to 6	V
Bridge Low-Side Source Terminals	$V_{LSS}$		-500 to 500	mV
		$t_w < 200\ \text{ns}$	-4 to 6	V
Junction Temperature	$T_j$		150	°C
Storage Temperature Range	$T_s$		-55 to 150	°C

[1] With respect to GND, unless otherwise noted. Ratings apply when no other circuit operating constraints are present.

[2] Lowercase "x" in terminal names and symbols indicates a variable sequence character.

**THERMAL CHARACTERISTICS:** May require derating at maximum conditions; see application information.

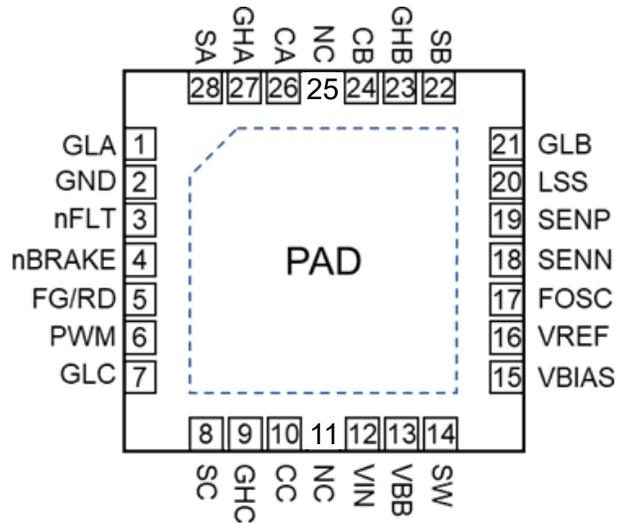
Characteristic	Symbol	Test Conditions [1]	Value	Unit
Package Thermal Resistance (Junction to Ambient)	$R_{\theta JA}$	28-contact QFN (package EC), on 2-sided PCB with 1 in <sup>2</sup> copper	45	°C/W
Package Thermal Resistance (Junction to Pad)	$R_{\theta JP}$		2	°C/W

[1] Additional thermal information is available on the Allegro website.

### RECOMMENDED OPERATIONAL RANGE

Characteristics	Symbol	Test Conditions	Min.	Typ.	Max.	Units
Power Supply Voltage	$V_{BB}$	DC	7	15	40	V
Logic Voltage Range	$V_I$	nBRAKE	-0.3	-	5.5	V
Operating Temperature Range	$T_a$		-40	-	105	°C

## PINOUT DIAGRAM AND TERMINAL LIST TABLE



EC Package (Top View)

### Terminal List Table

Number	Name	Function
1	GLA	Gate drive output
2	GND	Ground
3	nFLT	Logic output
4	nBRAKE	Logic input
5	FG/RD	Logic output; also used as SDA for I <sup>2</sup> C
6	PWM/SPD	Logic input; also used as SCK for I <sup>2</sup> C
7	GLC	Gate drive output
8	SC	Motor output
9	GHC	Gate drive output
10	CC	C <sub>BOOTSTRAP</sub>
11	NC	No connection
12	VIN	Analog input
13	VBB	Power supply input
14	SW	Switch node

Number	Name	Function
15	VBIAS	Voltage regulator output
16	VREF	Logic supply output
17	ROSC	Analog input
18	SENN	Current sense negative terminal
19	SENP	Current sense positive terminal
20	LSS	Low-side source
21	GLB	Gate drive output
22	SB	Motor output
23	GHB	Gate drive output
24	CB	C <sub>BOOTSTRAP</sub>
25	NC	No connection
26	CA	C <sub>BOOTSTRAP</sub>
27	GHA	Gate drive output
28	SA	Motor output

## ELECTRICAL CHARACTERISTICS <sup>[1]</sup>: Valid at $T_J = 25^\circ\text{C}$ , $V_{BB} = 15\text{ V}$ (unless noted otherwise)

Characteristics	Symbol	Test Conditions	Min.	Typ.	Max.	Units
Power Supply Voltage	$V_{BB}$	$V_{BB} = 40\text{ V}$	7 <sup>[2]</sup>	15	40	V
VBB Supply Current	$I_{BB1}$	Standby, $V_{IN} > V_{INTH}$ , $V_{BB} > V_{BBUVLO}$	–	6	–	mA
	$I_{BB2}$	$V_{IN} < V_{INTH}$	–	0.8	3.3	mA
VBIAS Output Voltage	$V_{BIAS}$	Buck regulator in use, $V_{BB} > 13\text{ V}$ , $I_{EXT\_LOAD} < 10\text{ mA}$	10	12.5	14	V
		$V_{BIAS}$ connected directly to $V_{BB}$ ( $\leq 15\text{ V}$ ), bypass buck regulator	7	$V_{BB}$	15	V
VREF	$V_{REF}$	$I_{EXT\_LOAD} < 5\text{ mA}$	1.7	1.8	1.9	V
VREF Current Limit	$V_{REFOCL}$	$V_{REF} = 0\text{ V}$ , internal current limit	70	92	135	mA
<b>GATE DRIVER</b>						
High-Side Gate Drive Output	$V_{GH}$	$V_{BB} = 40\text{ V}$ , DC; buck regular in use	9.3	11.8	13.3	V
		$V_{BB} = 15\text{ V}$ , DC; buck regulator is bypassed, $V_{BIAS} = V_{BB}$	–	$V_{BB} - 0.7$	–	V
Low-Side Gate Drive Output	$V_{GL}$	$V_{BB} = 40\text{ V}$ , DC; buck regular in use	10	12.5	14	V
		$V_{BB} = 15\text{ V}$ , DC; buck regulator is bypassed, $V_{BIAS} = V_{BB}$	–	$V_{BB}$	–	V
Gate Drive Source Current	$I_{SRC}$	PWMGDSLEWRATE = 0, DC, $V_{GS\_TH} = 3\text{ V}$	7	8.5	10	mA
		PWMGDSLEWRATE = 1, DC, $V_{GS\_TH} = 3\text{ V}$	19	25.5	32	mA
		PWMGDSLEWRATE = 2, DC, $V_{GS\_TH} = 3\text{ V}$	31	42	53	mA
		PWMGDSLEWRATE = 3, DC, $V_{GS\_TH} = 3\text{ V}$	48	63	78	mA
Gate Drive Sink Current	$I_{SNK}$	PWMGDSLEWRATE = 0, DC, $V_{GS\_TH} = 3\text{ V}$	16	23	30	mA
		PWMGDSLEWRATE = 1, DC, $V_{GS\_TH} = 3\text{ V}$	33	46	60	mA
		PWMGDSLEWRATE = 2, DC, $V_{GS\_TH} = 3\text{ V}$	50	68	87	mA
		PWMGDSLEWRATE = 3, DC, $V_{GS\_TH} = 3\text{ V}$	50	68	87	mA
GHx Passive Pull-Down	$R_{GHPD}$	$V_{BB} = 0$ , $V_{GHx} - V_{Sx} < 0.1\text{ V}$	0.5	–	2	M $\Omega$
GLx Passive Pull-Down	$R_{GLPD}$	$V_{BB} = 0$ , $V_{GLx} - V_{LSS} < 0.1\text{ V}$	0.5	–	2	M $\Omega$
<b>PROTECTION CIRCUITS</b>						
Lock Protection	$t_{OFF}$	Relative to programmed target, ROTSTARTRETRYTOUT	–10	–	10	%
Overcurrent Limit	$I_{OCL}$	Relative to programmed target, SFOCDRVCURRLMT	–15	–	15	%
Thermal Shutdown Temp.	$T_{JTSD}$	Temperature increasing	145	160	175	$^\circ\text{C}$
Thermal Shutdown Hysteresis	$\Delta T_J$	Recovery = $T_{JTSD} - \Delta T_J$	–	20	–	$^\circ\text{C}$
VREF UVLO	$V_{REFUVLO}$	$V_{BIAS}$ rising	1.35	1.45	1.55	V
VBB UVLO	$V_{BBUVLO}$	$V_{BB}$ rising, UVSTH = 0	29	30	32	V
		$V_{BB}$ rising, UVSTH = 1	23	24	25	V
		$V_{BB}$ rising, UVSTH = 2	6.2	6.7	7.5	V

<sup>[1]</sup> Specified limits are tested at a single temperature and assured over operating temperature range by design and characterization.

<sup>[2]</sup> When  $V_{BB} < 13\text{ V}$  and a buck regulator is in use, gate drive output voltage tracks  $V_{BB}$  voltage.

**ELECTRICAL CHARACTERISTICS (cont.)** [1]: Valid at  $T_J = 25^\circ\text{C}$ ,  $V_{BB} = 15\text{ V}$  (unless noted otherwise)

Characteristics	Symbol	Test Conditions	Min.	Typ.	Max.	Units
<b>POWER LOSS BRAKE</b>						
$V_{IN}$ Logic Threshold	$V_{INTH}$	$V_{IN}$ falling	–	2.7	–	V
Hysteresis	$V_{INHYS}$		–	500	–	mV
$V_{IN}$ Pull-Down Resistor	$V_{INPD}$		–	870	–	k $\Omega$
$V_{BB}$ Regulated Boost Voltage	$V_{BOOST}$	$V_{IN} < V_{INTH}$	7.4	8.1	8.9	V
$V_{BB}$ Boost Low Threshold	$V_{BBTH}$		–	1.1	–	V
Boost Switching Frequency	$f_{BOOST}$	Subject to change	–	40	–	kHz
<b>LOGIC INPUTS AND OUTPUTS</b>						
Logic Input Low Level	$V_{IL}$	nBRAKE	0	–	0.8	V
Logic Input High Level	$V_{IH}$	nBRAKE	2	–	6	V
Logic Input Hysteresis	$V_{HYS}$	nBRAKE	200	300	600	mV
Logic Input Current	$I_{IN}$	SPD, nBRAKE	–10	< 1	15	$\mu\text{A}$
Output Saturation Voltage (FG/RD, nFLT)	$V_{SAT}$	$I = 1\text{ mA}$	–	–	0.3	V
Output Leakage (FG/RD)	$I_O$	$V = 12\text{ V}$ , switch OFF	–	–	5	$\mu\text{A}$
Output Leakage (nFLT)	$I_O$	$V = 6\text{ V}$ , switch OFF	–	–	10	$\mu\text{A}$
<b>INTERNAL OPEN-DRAIN PULL-UP</b>						
Internal Pull-Up Voltage		FG/RD; $V_{BB} = 40\text{ V}$ , DC; buck regulator in use	10	12.5	14	V
		FG/RD; $V_{BB} = 15\text{ V}$ , DC; buck regulator is bypassed, $V_{BIAS} = V_{BB}$	–	$V_{BB}$	–	V
		nFLT, nBRAKE	4.25	5	5.75	V
		PWM/SPD	3.75	4	4.25	V
Internal Pull-Up Resistor		FG/RD	12	20	28	k $\Omega$
		PWM/SPD, nFLT, nBRAKE	60	100	140	k $\Omega$
<b>I<sup>2</sup>C TIMING</b>						
SCL Clock Frequency	$f_{CLK}$		10	–	400	kHz
Bus Free Time Between Stop/Start	$t_{BUF}$		1.3	–	–	$\mu\text{s}$
Hold Time Start Condition	$t_{HD:STA}$		0.6	–	–	$\mu\text{s}$
Setup Time for Start Condition	$t_{SU:STA}$		0.6	–	–	$\mu\text{s}$
SCL Low Time	$t_{LOW}$		1.3	–	–	$\mu\text{s}$
SCL High Time	$t_{HIGH}$		0.6	–	–	$\mu\text{s}$
Data Setup Time	$t_{SU:DAT}$		100	–	–	ns
Data Hold Time	$t_{HD:DAT}$		0	–	900	ns
Setup Time for Stop Condition	$t_{SU:STO}$		0.6	–	–	ms

**ELECTRICAL CHARACTERISTICS (cont.)** [1]: Valid at  $T_J = 25^\circ\text{C}$ ,  $V_{BB} = 15\text{ V}$  (unless noted otherwise)

Characteristics	Symbol	Test Conditions	Min.	Typ.	Max.	Units
<b>SPEED CONTROL</b>						
PWM Duty Input, for PWM Duty Control Mode	$f_{\text{PWM}}$		0.1	–	100	kHz
	$t_{\text{PWM(LOW)}}$	PWM low minimum pulse width	100	–	–	ns
Duty Cycle On Threshold	$\text{DC}_{\text{ON}}$	Relative to programmed target	–0.5	–	0.5	%
Duty Cycle Off Threshold	$\text{DC}_{\text{OFF}}$	Relative to programmed target	–0.5	–	0.5	%
Analog SPD Full-Range Voltage, for Analog External Command Source (Analog Control Mode)	$\text{AnaSpd}_{\text{MAX}}$	$I_{\text{LOAD}} = 10\ \mu\text{A}$	0	–	3.6	V
Analog SPD Resolution			–	1	–	mV
Input Clock Frequency Range (Clock Mode)		Relative to programmed target, CLKCOMPREF	0.1	–	1	kHz
Speed Setpoint (Digital, Not Clock Mode)	$F_{\text{SPD}}$	$R_{\text{OSC}} = 25\ \text{k}\Omega$ (0.1%)	–2.5	–	2.5	%
Speed Setpoint (Digital, Clock Mode)	$F_{\text{SPDCLK}}$	PWM input frequency = CLKCOMPREF $\pm 0.05\%$	–0.1	–	0.1	%
System Oscillator	$f_{\text{OSC}}$	$R_{\text{OSC}} = 25\ \text{k}\Omega$ (0.1%)	24.5	25	25.5	MHz
<b>ID CLOCK TIMING</b>						
Maximum ID Clock Time	$t_{\text{idmax}}$	Relative to programmed target, FGIDDUR	–10%	–	10%	s
ID Clock Frequency	$f_{\text{idclk}}$	Relative to programmed target, FGIDFREQ	–5%	–	5%	Hz
$V_{\text{BB}}$ UVLO to ID Clock Delay	$t_{\text{diy1}}$	Relative to programmed target, FGIDFREQ	–	–	5%	s
PWM Rising Edge to End of ID Clock	$t_{\text{diy2}}$	Relative to programmed target, FGIDFREQ	–	–	5%	s
<b>NONVOLATILE MEMORY (NVM) PROGRAMMING</b>						
Minimum $V_{\text{BB}}$ for Programming	$V_{\text{NVM Prog}}$	$V_{\text{BB}}$	25	–	–	V

**PIN DESCRIPTIONS****VBB**

Main power supply for internal regulators. Tie the VBB pin to the GND pin using a low-equivalent series resistor (ESR) ceramic bypass capacitor of 0.1  $\mu$ F. This capacitor should be situated as close as possible to the VBB pin with a thick trace.

**VIN**

The VIN input is used to sense the supply voltage for the power-loss braking (PLB) function. The PLB function becomes active if the voltage on this input reduces to less than  $V_{INTH}$ . VIN must be connected to the power supply on the anode side of the blocking diode shown in Figure 1.

**VREF**

Voltage reference (1.8 V) to power internal digital logic. A low-ESR ceramic capacitor with 4.7  $\mu$ F or greater is required on the pin to stabilize the supply. This regulator can supply up to 5 mA externally.

**VBIAS**

Internal buck regulator output. Connected to external inductor and output capacitor. VBIAS provides supply current for gate drive, digital logic, bootstrap capacitors, and low-voltage analog circuitry. Up to 10 mA can be externally sourced from the VBIAS pin.

**SW**

Buck regulator switching node connected to inductor and rectifier diode.

**FG/RD**

FG/RD is an open-drain output that can be pulled up to VBB externally. It also has by default an internal pullup to 12V that can be disabled through IPUP\_FGRD\_DIS parameter in NVM. The selection of function is programmed via NVM parameters as well to provide either speed (FG) or rotation detection (RD) data. For more information, refer to the FG/RD Pin Section.

The FG/RD pin is also used as a serial data (SDA) port in the I<sup>2</sup>C mode.

The I<sup>2</sup>C command can pass only when this pin is high (open drain).

**PWM/SPD**

Device control demand input. Supports analog, PWM, or frequency command.

It also has, by default, an internal pullup to 4 V that can be disabled through IPUP\_PWMSPD\_DIS NVM parameter. The PWM/SPD pin is also used as SCK in the I<sup>2</sup>C mode.

**ROSC**

The ROSC terminal is used to improve the accuracy of the internal system clock for better accuracy control of motor speed. To use this feature, connection of a 0.1% 25 k $\Omega$  resistor between the ROSC terminal and GND is recommended. A 1% resistor can be used for applications where speed control accuracy is not critical.

**Sx**

Load phase connections. These terminals are the negative supply connections for the floating high-side drivers and are also connected to the negative side of the bootstrap capacitors.

**Cx**

High-side connections for the bootstrap capacitors and positive supply for high-side gate drivers.

**GHx**

High-side, gate-drive outputs for external N-channel MOSFETs.

**GLx**

Low-side, gate-drive outputs for external N-channel MOSFETs.

**LSS**

Low-side return path for discharge of the capacitance on the MOSFET gates, connected to the common sources of the low-side external MOSFETs through a low-impedance track.

**SENN**

Current sense negative terminal.

**SENP**

Current sense positive terminal.

## nBRAKE

This is the active low-input signal. It turns on all low sides for the braking function. The brake function overrides input control. Brake input is ignored during a thermal shutdown (TSD) event or  $V_{BB} < V_{BBUVLO}$ . Care should be taken to avoid stressing the MOSFET when braking while the motor is running.

When braking, the current is limited only by  $V_{BEMF}/R_{MOTOR}$ . The A89333-1 includes an optional feature that delays braking until the motor speed reduces to a level that is sufficiently low (configurable `BRAKE_FREQ_TOO_HIGH_TH` parameter in NVM) that the braking current does not damage the MOSFET.

The nBRAKE pin also has, by default, an internal pull-up to 5 V that can be disabled through the `IPUP_NBRAKE_DIS` parameter in NVM.

## nFLT

This open-drain output provides the fault status of the motor operation.

This pin is internally pulled up to 5 V by default. Pull-up can be disabled through NVM. The default is high when there is no fault. When a fault is detected, the nFLT pin transitions to low and remains active (low) until the fault is cleared according to the latched or not-latched mechanism.

The nFLT fault reporting function is enabled by default, but it can be disabled by selecting `NFLT_DIS = 1` in the NVM.

The nFLT feature can be used to indicate a successful software startup after POR by being low for a short period of time as detailed in Figure 3.

This feature can be enabled/disabled in the CONFIG register of the NVM using `NFLT_STARTUP_DIS`.

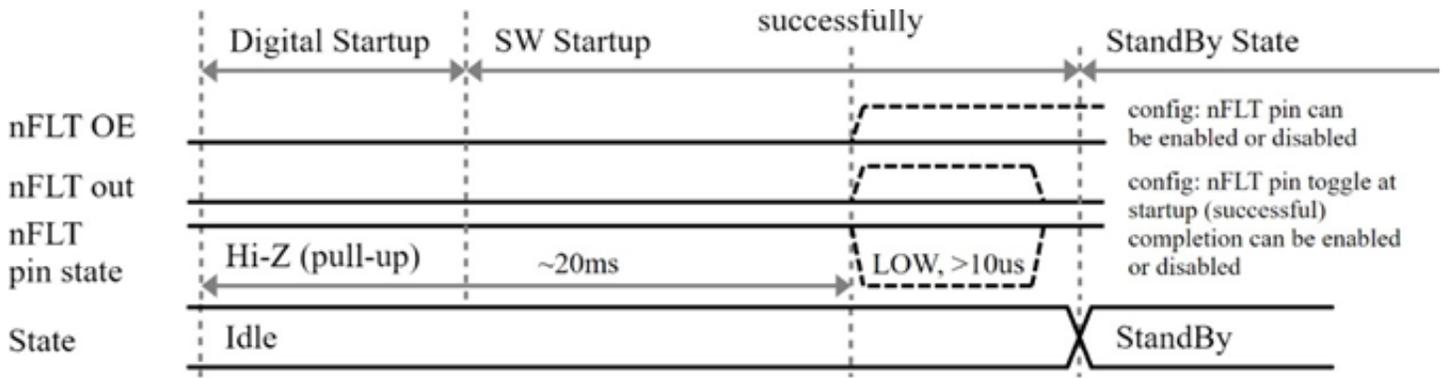


Figure 3: nFLT Pin at Startup



## External Command Source

The A89333-1 can be controlled with five different sources of command according to the EXT\_CMD\_SRC in the NVM register setting.

### ANALOG INPUT VOLTAGE (EXT\_CMD\_SRC, 0X1).

Motor command is proportional to the analog voltage applied on the PWM/SPD pin.

Direction data, when available, is defined in the NVM and the UCC. For further information, refer to the Motor Rotation Direction section.

The analog command is converted into the digital domain and is rescaled according to:

Equation 1:

$$mca_{extcommand} = (2^{15} - 1) \times \frac{V_{PWM/SPD}}{AnaSpd_{Max}}$$

where  $AnaSpd_{Max}$  is a fixed voltage equal to 3.6 V. For example, see Table 1.

### PWM DUTY CYCLE (EXT\_CMD\_SRC, 0X2)

Motor control is proportional to the duty cycle applied on the PWM/SPD pin. The frequency range of the input PWM is from 100 Hz to 100 kHz. There is a 100 ns minimum PWM low pulse limit with this mode, which means the IC cannot detect PWM low pulse less than 100 ns reliably and function correctly.

Direction data, when available, is defined in the NVM and the

UCC. For further information, refer to the Motor Rotation Direction section.

The duty cycle command is converted into the digital domain according to:

Equation 2:

$$mca_{extcommand} = (2^{15} - 1) \times duty.$$

For example, see Table 2.

In this mode, it is possible to enable the clock mode feature to synchronize the internal clock with the external PWM signal frequency. This can provide higher speed accuracy and can eliminate the need for a precision external resistor on the ROSC terminal. The external PWM signal is used to compensate for the inaccuracy of the integrated oscillator, allowing speed accuracy to be achieved down to 0.1%. When this feature is activated (CLK\_COMP\_ENABLE), the input admissible frequencies of the external PWM signal are fixed and need to be specified in the CLK\_COMP\_REF register. To detect the frequency, the input duty cycle of the PWM signal must be greater than 0% and less than 99%. If a 0% or 100% duty cycle value is applied, the clock compensation is not applied. Speed accuracy is directly related to the accuracy of the PWM clock frequency to the selected CLK\_COMP\_REF frequency.

Table 1: Conversion from Analog Input Voltage to Digital Command

duty <sub>PWM/SPD</sub> (V)	mca <sub>extcommand</sub> (LSB) AnaSpd <sub>Max</sub> = 3.6 V
0.5	4551
2.5	22755
3.6	32767

Table 2: Conversion from PWM Input Duty to Digital Command

duty <sub>PWM/SPD</sub> (%)	mca <sub>extcommand</sub> (LSB)
25	8192
50	16384
75	24575

## FREQUENCY MODE (EXT\_CMD\_SRC, 0X3)

Motor control is proportional to the frequency applied on the PWM/SPD pin. The input frequency range needs to be between 44.5 and 2666 Hz (duty cycle is intended to be 50%, but this mode works with any setting other than 0 or 100%).

If PWM input frequency is greater than 2666 Hz, MCA\_EXT\_COMMAND assumes the maximum value equal to 32767 [LSB]. If PWM input frequency is less than 44.5 Hz, MCA\_EXT\_COMMAND is equal to 0.

Direction data, when available, is defined in the NVM and the UCC. For further information, refer to the Motor Rotation Direction section.

The frequency command is converted into the digital domain according to:

Equation 3:

$$mca_{extcommand} = (pwm_{freq} [Hz] - 44.5) \times map_{coefficient}$$

where  $map_{coefficient}$  is a scaling factor equal to 12.496. For example, see Table 3.

**Table 3: Conversion from PWM Input Duty to Digital Command**

frequency <sub>PWM/SPD</sub> (Hz)	mca <sub>extcommand</sub> (LSB)
44.5	0
100	$(100 - 44.5) \times 12.496 = 694$
200	$(200 - 44.5) \times 12.496 = 1943$
2666	$(2666 - 44.5) \times 12.496 = 32758$

## I<sup>2</sup>C MODE (EXT\_CMD\_SRC, 0X0)

The motor control speed reference command is defined by writing in the REF\_CMD register through I<sup>2</sup>C protocol. The I<sup>2</sup>C clock, SCK, is mapped on the PWM/SPD pin, and I<sup>2</sup>C data is mapped on the FG pin. In this mode, the motor electrical frequency can be read through the register, as well as many other internal parameters.

The value selected in REF\_CMD is copied into MCA\_EXT\_COMMAND. Direction data, when available, is defined in the NVM and UCC.

The A89333-1 can load a predefined command into the MCA\_EXT\_COMMAND register at power-up (POR) to start the motor without the need for an external command. The default command can be set in DEFAULT\_EXT\_CMD in the NVM and, at power-up, its value is copied into the MCA\_EXT\_COMMAND register. To disable this feature, DEFAULT\_EXT\_CMD must be set to 0.

The command is treated as speed, power, or torque, depending on the mode selected.

When FG is in the high state (not driven) or when the device has been configured in analog, PWM, or frequency external command source, I<sup>2</sup>C communication is always available.

I<sup>2</sup>C data is mapped on the FG pin and, because the pin is an open drain, it can be controlled by the I<sup>2</sup>C when in the high state. The internal NVM register, shadow NVM register, and status register can therefore be read and set during typical operation. However, for reliable communication, use of I<sup>2</sup>C is recommended when the A89333-1 is in the standby state (motor stopped).

NOTE 1: The internal NVM register and the shadow NVM register are inaccessible in application operation mode. They can be accessed only in user operation mode or in test operation mode. For more information, refer to the Operation Modes and Customer Password Protection section.

NOTE 2: The I<sup>2</sup>C SCK signal on the PWM/SPD pin is interpreted to be the maximum command. This is because, during serial transactions, the pin state is high, which is a valid command that is therefore interpreted as the maximum command.

For reliable communication, it is better to use serial communication in the UV mode to prevent issues related to motor start and proper FG/RD pin state.

For more information, refer to the VBB, UV, and NVM Reprogramming section.

## Universal Curve Controller: UCC

The MCA\_EXT\_COMMAND motor command is passed through a universal curve controller to create an arbitrary command profile, then to the FOC algorithm. The input of the UCC is unsigned(MCA\_EXT\_COMMAND [LSB]) and the output is signed(MCA\_EXT\_COMMAND [LSB]), as shown in Figure 5.

The UCC is a transformer curve defined by corner points. Each point has a specific input value and corresponding output value. Values between points are calculated using linear interpolation. Up to 10 corner points can be defined in NVM (UCC\_X0 to UCC\_Y9). Corner points do not all require definition—only as many as are needed for the desired curve.

A closed-loop nonoperational region, defined by the PO\_OPER parameter in the NVM, marked in the red hatched rectangular area in Figure 4, defines the minimum speed operation for reliable position-observer estimation and proper FOC functionality. Because operation in this area is not reliable, programming the UCC in this area is not recommended. The easiest way to prevent operation in this area is to use hysteresis, as shown in Figure 5.

Some examples of demand curves using screenshots taken from the GUI application follow.

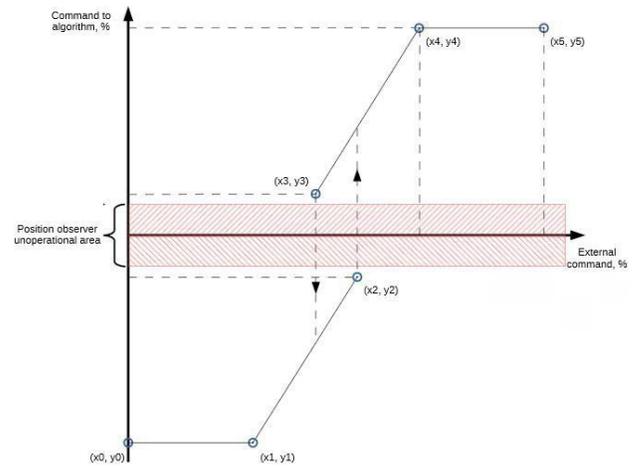
**Example 1:** The default setting in which the output (Y axis) is same as the input (X axis) is shown in Figure 6. This curve can be used if the transformer is not needed.

**Example 2:** When the control loop is set to closed-loop speed, the example shown in Figure 7 can be used to avoid the resonant frequency of the motor, if needed.

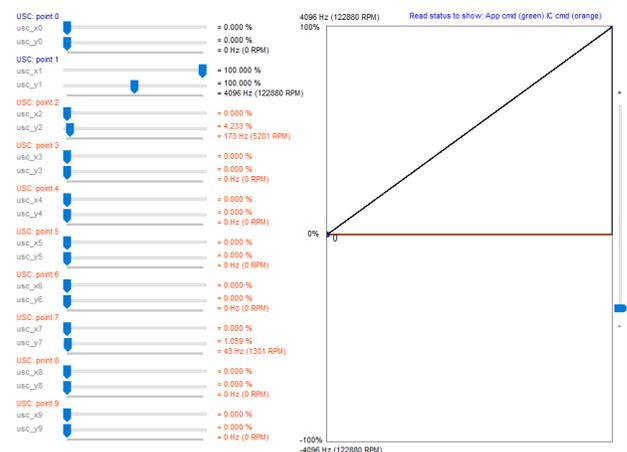
**Example 3:** Hysteresis can be implemented by setting the input value of an address lower than the input value in the previous address. In this example shown in Figure 8, as the input demand rises, the output demand jumps to the next higher level at the vertical lines on the right of each transition. When the input demand falls, the output demand drops to the next lower level following the vertical lines on the left of each transition. This prevents output jitter when the input is around a boundary.

**Example 4:** In this example shown in Figure 9, the motor does not turn on until the input is approximately 23% and does not turn off until the output falls below about 20%. When the input is between about 90% to 96%, the output is at 10.6% (13002 rpm); when the input is greater than 96%, the motor stops.

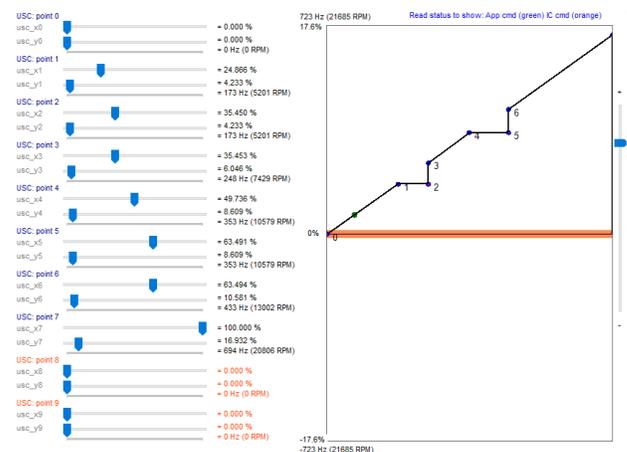
**Example 5:** The curve can be used when bidirectional operation is required. In this case, when input is at 0%, the motor is at the selected maximum speed in the reverse direction; when the input is at 100%, the motor is at the maximum speed in the forward direction; and the motor is stopped when the input is approximately 50%. See Figure 10.



**Figure 5: UCC Transfer Function from External Command to FOC Command**



**Figure 6: UCC Default Curve, Example 1**



**Figure 7: UCC Example 2**

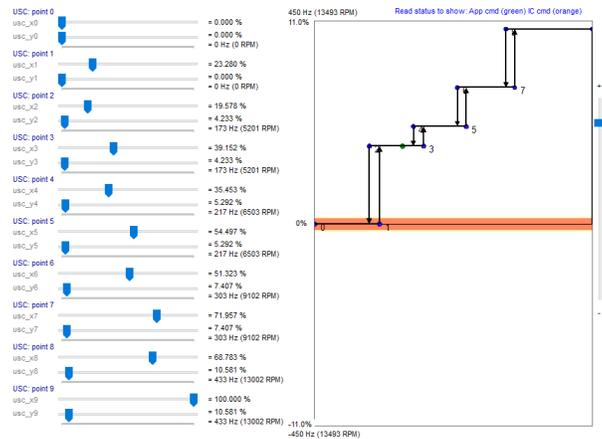


Figure 8: UCC Example 3

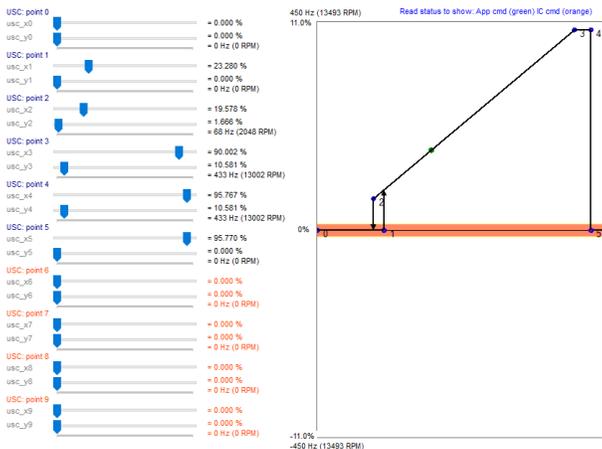


Figure 9: UCC Example 4

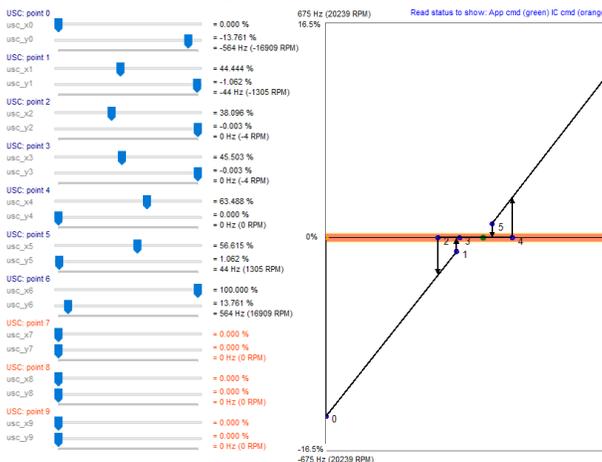


Figure 10: UCC Example 5

## Motor Rotation Direction

Information about direction is decoupled from MCA\_COMMAND. As shown in Figure 3, the FOC algorithm has two inputs: direction and command.

The direction of the motor depends on:

- Direction bit in the REF\_CMD register, REF\_CMD[16]
- MSB of MCA\_COMMAND, MCA\_COMMAND[16]:
  - If the Y values of the UCC are all positive, then MCA\_COMMAND[16] = 0; otherwise, MCA\_COMMAND[16] = 1
- ROT\_DIR\_INVERT configurable NVM parameter
- Operation control mode (speed, power, torque mode, selected according to SFOC\_VAR\_CTRL\_MODE).

In speed control mode, motor direction is defined by:

- Motor direction = MCA\_COMMAND[16] XOR ROT\_DIR\_INVERT XOR REF\_CMD[16]

In torque and power control mode, motor direction is defined by:

- Motor direction = ROTDIRINVERT XOR REF\_CMD[16]
- For torque and power control mode, ensure MCA\_COMMAND[16] is 0 by setting Y values to all positive values.

## Speed, Torque, or Power Control Modes

A89333-1 includes a control loop able to support three operational modes for motor control: speed, torque, and power. The control variable can be selected with the SFOC\_VAR\_CTRL\_MODE NVM register setting.

### Speed Mode (0x0)

In speed mode, MCA\_COMMAND is used as a reference for the FOC speed loop to regulate the motor speed to  $f_{ref}$  [Hz].

MCA\_COMMAND is scaled to the maximum frequency [Hz] according to the following formula:

Equation 4:

$$f_{ref}[W] = mca_{command}[LSB] \times \frac{f_{max} [Hz]}{2^{15} - 1 [LSB]}.$$

### Torque Mode (0x2)

In torque mode, MCA\_COMMAND is used as reference for the FOC current loop to regulate the motor torque proportional to  $I_{ref}$  [A].

In this mode, the FOC speed loop is bypassed and the reference command is compared directly with estimated q axis current,  $I_{qref}$ .

MCA\_COMMAND is scaled to the maximum system current [A] according to:

Equation 5:

$$I_{ref}[W] = mca_{command}[LSB] \times \frac{i_{max} [A]}{2^{15} - 1 [LSB]}.$$

In torque control mode, MCA\_COMMAND is downscaled to the current fraction length (11 bits). For this reason, the FOC algorithm command changes only if the external command varies for more than 16 units.

### Power Mode (0x1)

In power mode, MCA\_COMMAND is used as a reference for the FOC power loop to regulate the motor power to  $P_{ref}$  [W].

MCA\_COMMAND is scaled to the maximum system power [W] according to:

Equation 6:

$$P_{ref}[W] = mca_{command}[LSB] \times \frac{P_{max} [W]}{2^{15} - 1 [LSB]}.$$

In power control mode, the command is down-scaled to the voltage fraction length (14 bits) and, for that reason, the FOC algorithm command changes only if the external command varies for more than 2 units.

## Maximum System Speed

The maximum system speed ( $f_{max}$  [Hz]) is the maximum electrical motor speed that can be commanded. It depends on frequency resolution,  $f_{res}$ , according to:

Equation 7:

$$f_{max} = round(2^{15} \times f_{res}),$$

where  $f_{res}$  [Hz/LSB] is the frequency resolution, set through the SFOC\_FREQ\_RES register according to:

Equation 8:

$$f_{res} = \frac{1 [Hz]}{9 \times 2^{sfocFreqRes} [LSB]}.$$

NOTE: The maximum rotation speed can be limited by supply voltage ( $V_{BB}$ ); therefore, high command speed may not result in high motor rotation due to low  $V_{BB}$  voltage.

## Maximum System Current and Bus Current Sensing

The maximum system current is typically set to 110% of the motor-rated current.

A single shunt resistor connecting between SENN and SENP is used to measure the bus current for the FOC algorithm and current limit. The resistor value is typically approximately tens of milliohms, depending on the maximum rated current of the system and the selected gain of the current sense amplifier.

Equation 9:

$$i_{max}[A] = \frac{ADC_{VREF}}{R_{shunt} \times CSA_{GAIN}},$$

where  $ADC_{VREF}$  is the reference ADC voltage equal to 1.2 V,  $R_{shunt}$  [ $\Omega$ ] is the board shunt resistance, and  $CSA_{GAIN}$  is the sense amplifier gain that can be set in the SFOC\_CSA\_GAIN NVM parameter to 10 V/V or 20 V/V.

Use of a Kelvin sensing connection is recommended when using the shunt resistor, as shown in Figure 11.

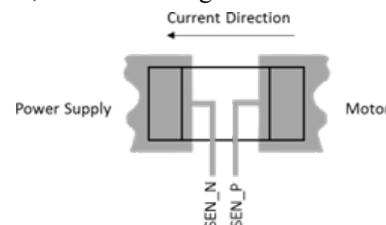


Figure 11: Kelvin Sensing Connection Recommended for Shunt Resistor Setups

## DC-Link Voltage

To enable proper controller operation, set the nominal DC-link voltage in the VBB\_NOM NVM parameter according to:

Equation 10:

$$VBB_{nom} = \text{round} \left( \frac{VBB_{nom}[V]}{0.515625} \right),$$

where  $VBB_{nom}$  [V] is the nominal DC-link voltage and 0.515625 [V] is the scaling factor.

NOTE: Proper functioning of the A89333-1 requires that the nominal VBB used to power the device is correctly configured in the VBB\_NOM NVM.

## Maximum Electrical Power

The maximum electrical power value [W] is calculated using:

Equation 11:

$$P_{max}[W] = \frac{3}{2} i_{max} 1.1547 \frac{VBB_{nom} [V]}{2}.$$

For example, with maximum system current,  $I_{Max}$ , of 6.25 A and  $VBB_{nom}$  of 12 V, the maximum electrical power is 64.95 W.

## SPEED LIMIT

The SFOC\_FREQ\_LMT NVM parameter limits the maximum rotation speed. It works for all speed, torque, and power, and it is normally used in power and torque modes.

## POWER LIMIT

The SFOC\_PWR\_LMT parameter in NVM limits the maximum power. This parameter is useful when commanding in torque and speed modes.

## CURRENT LIMIT

The SFOC\_DRV\_CURR\_DRV\_LMT parameter in NVM limits the  $I_q$ , which subsequently limits the  $I_{BB}$ . This parameter is useful when commanding in power and speed modes.

## Motor Control Application (MCA) Finite State Machine (FSM)

A89333-1 implements the FOC algorithm through a state machine, composed of four modes and six distinct states. The four modes of the MCA (motor controller application) are:

1. Standby Mode—This mode is activated after completion of

the system startup routine or receipt of the command to stop motor driving (motor control application FSM enters SBY state, as described next).

2. Rotate Mode—This mode is activated when a command to start the motor is received (on exit from the SBY state).
3. Brake Mode—This mode is activated when a command to brake the motor is received.
4. Fail Mode—This mode is activated when one of the enabled faults is detected. Active fail mode is reported by activation of the nFLT pin.

The active mode of MCA can be read in the SW status register via I<sup>2</sup>C communication.

The distinct states of the MCA FSM are shown in Figure 12:

- A89333-1 powers up in the standby state (SBY) with external power bridge in tri-state mode.
- After the internal initialization is complete and once a command to run the motor is received, the A89333-1 transitions to the windmill check state (WNDML) to determine the initial status of motor movement and then start to drive the motor as shown in Figure 12.
- If the motor is stationary or spinning at a very low speed that is considered to be stationary (typical startup), the A89333-1 enters the IPD state or the align state—depending on the NVM option (ALIGN\_TYPE) to determine the initial rotor position or to put rotor into a known position—followed by the open-loop ramp-up (RAMPUP) and drive states.
- If the motor spins in the reverse direction (reverse windmill), braking (BRAKE mode) or deceleration with FOC control is applied to stop the motor.
- Once the motor stops, the typical startup routine can be applied as before.
- If the motor is already rotating in the correct direction (forward windmill), depending on the NVM option (described in the Windmilling—WNDML section), the driver can enter the drive state directly, skipping the IPD/align state and the ramp-up phase, or braking/FOC deceleration can be used to stop the motor, such as the reverse windmill, followed by typical startup.

The active state of the MCA can be read in the SW status register via I<sup>2</sup>C communication.

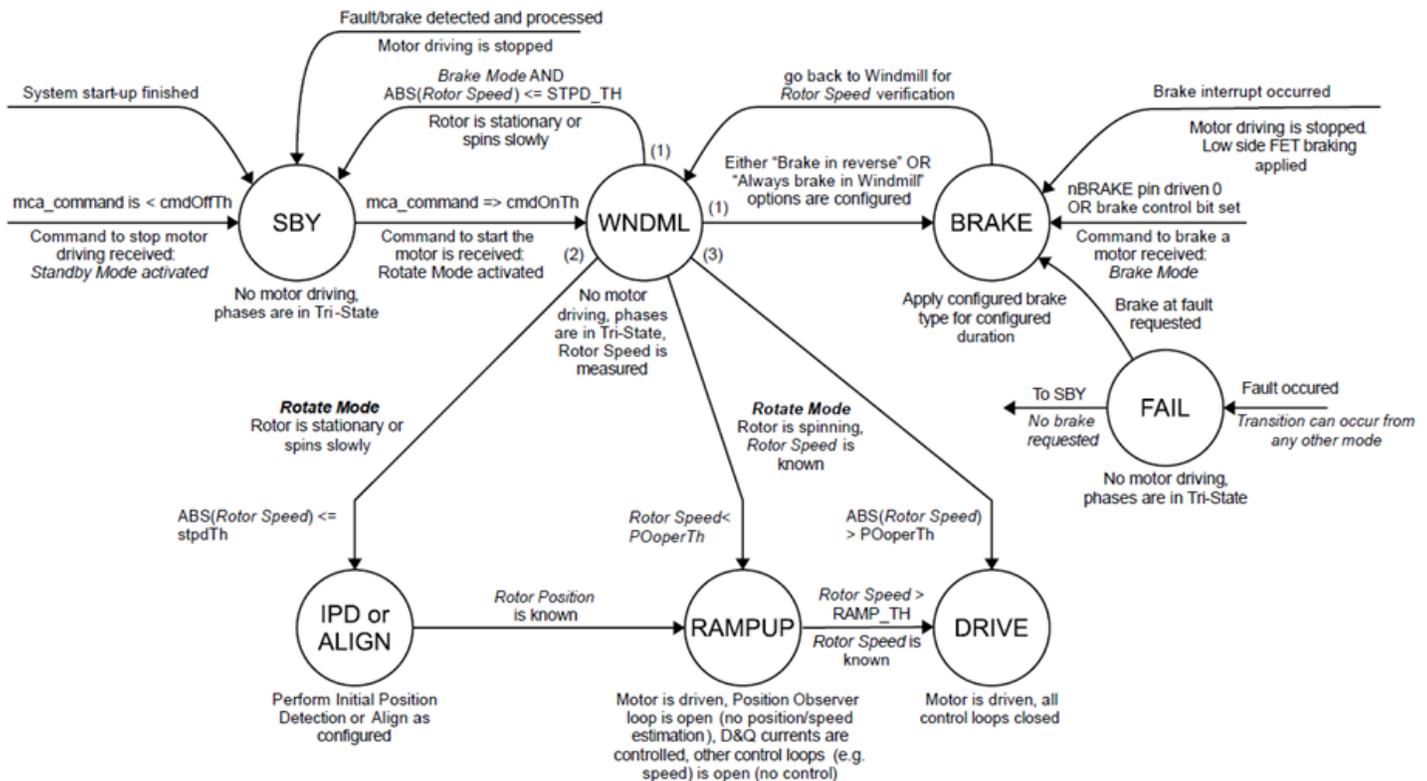


Figure 12: MCA FSM States

## STANDBY—SBY

In the SBY state, the motor is not driven, and the power stage is in tri-state, so the motor can be externally rotated.

The A89333-1 transitions to the windmill (WNDML) state only when MCA\_COMMAND exceeds the command on threshold of CMD\_ON\_TH and returns to standby when MCA\_COMMAND is less than the command off threshold of CMD\_OFF\_TH.

The A89333-1 enters standby mode when one of the following conditions is verified:

- After completion of the system startup routine.
- At any point in time (independently, based on current state) after a fault is processed in the fail state.
- In brake mode, after the rotor successfully stops.
- If MCA\_COMMAND reduces to less than CMD\_OFF\_TH. This is the procedure for commanding the motor to stop.

## WINDMILLING—WNDML

In this state, the motor is not driven; however, the back electro-magnetic force (BEMF) signals from the windings of the motor is analyzed to determine the rotation speed of the motor, the position of the rotor, and the direction of movement.

Based on the rotor speed measurement, the state machine reacts as follows:

- If the motor speed is less than the stopped threshold (STPD\_TH, NVM parameter) or if an illegal switching sequence is detected, the device enters initial position detection (IPD) or rotor alignment (ALIGN) to determine the rotor position.
- If motor rotation exceeds the stopped threshold (STPD\_TH) and:
  - Motor rotation is in the proper direction:
    - ◆ If the brake is enabled during the windmill state (BRAKE\_IN\_WNDML\_ALWAYS\_EN = 1, NVM parameter), the device enters the BRAKE state to reduce speed. The brake pattern is applied until the rotor is stationary. When speed is less than STPD\_TH, the device enters the standby state.

- ◆ If the brake is not enabled during the windmill state, the device enters the drive or ramp-up state, depending on the absolute value of the speed value with respect to the observer operational threshold (PO\_OPER, configurable NVM parameter).
- Motor rotation is in the improper direction:
  - ◆ If the brake is enabled in the windmill state (BRAKE\_IN\_WNDML\_ALWAYS\_EN = 1 or BRAKE\_IN\_REVERSE\_TYPE = 1), the device enters the brake state to reduce speed. From the brake state, the device returns to the windmill state to verify the speed condition. When the speed is less than STPD\_TH, the device enters the standby state.
  - ◆ If the brake is not enabled in the windmill state, the motor is decelerated by FOC. Once it stops, it restarts in the opposite direction.

## IPD AND ALIGN

The startup of a motor from stationary requires a known rotor position. A89333-1 supports both initial position detection (IPD) and alignment techniques.

- IPD (ALIGN\_TYPE = 1, configurable NVM parameter), initial rotor position is determined by measuring the stator inductance difference caused by rotor flux. The IPD technique offers smoother and faster startup, without reverse spinning by using salient characteristics and winding saturation characteristics to determine the rotor position. IPD is performed in two stages:
  - In the first stage, test-pulse sequences are applied to the motor. If there is sufficient saliency ( $L_q \neq L_d$ ), A89333-1 locks the rotor position within 30° of 0° to 180° or 180° to 360°.
  - When the first stage completes, A89333-1 applies a test sequence that uses the saturation property of the phase inductances of the motor to determine the current magnetic polarity of the rotor. Once the entire sequences complete, A89333-1 can determine the rotor angle within 30° accuracy.
- Align mode (ALIGN\_TYPE = 0). A89333-1 supports both AC and DC alignment.
  - DC alignment is enabled by configuring SFOC\_ACDC\_ALIGN\_TYPE = 0. A DC current is injected for a fixed length of time that is configured by the SFOC\_ALGN\_TIME parameter, such that the rotor aligns with the stator in a known position. The current limit during DC alignments is configured through the SFOC\_ALGN\_D\_CURR\_REF parameter. The SFOC\_ALGN\_TIME and SFOC\_ALGN\_D\_CURR\_REF parameters are generally related to the inertia of the system, and it is advisable to increase these two parameters if the inertia is large or if a load is applied on the shaft.
  - AC alignment is enabled by configuring SFOC\_ACDC\_ALIGN\_TYPE = 1. A low-current-controlled driving frequency is applied to the winding to generate a known-position flux in the rotor. The integrated permanent magnet rotor gravitates to the generated stator flux. The AC alignment mode spins the rotor in open-loop control mode for the configured amount of time (ALGN\_DUR, SFOC\_ALGN\_TIME) with constant frequency (AC\_ALGN\_FREQ, 1/ALGN\_DUR) and current reference (SFOC\_ALGN\_D\_CURR\_REF). The alignment period should be chosen to match with the load torque required to gravitate the rotor. Longer alignment periods are more likely to catch the rotor than shorter alignment periods.

In align mode, the rotor may oscillate for some time before it starts to accelerate. This mode is typically used when the rotor position cannot be detected by the IPD. It is also a default action if the IPD fails to detect the initial rotor position (IPD\_FAIL\_ACTION).

After alignment or IPD completes, the FOC algorithm assumes that the rotor is stationary and is in the expected position, and the device enters the ramp-up state.

## RAMP-UP—RAMPUP

During ramp-up, the driving frequency increases in open-loop mode until sufficient BEMF is generated to allow the observer to accurately detect the rotor speed and position for the transition into the closed-loop state (drive state).

Open-loop ramp-up increases rotor frequency up to RAMP\_UP\_FREQ based on the following parameters:

- SFOC\_RAMP\_TIME, which defines the length of the ramp-up phase.
- SFOC\_RAMP\_STEP, which defines the acceleration [freq/s] during the ramp-up phase only.
- SFOC\_RUP\_D\_CURR\_REF, which defines the current during ramp-up. Ramp-up speed is not affected by the value of the current. The appropriate current level depends on the properties of the motor and the connected load.

The choice of SFOC\_RAMP\_STEP and SFOC\_RAMP\_TIME affects the frequency of occurrences of transitions between open-loop and closed-loop states.

For reliable start-up, an OL-CL transition frequency greater than 35 Hz is advised. This is achieved by selecting: 1) a RAMP\_STEP value that is not excessively large, to allow use of a current equal to 60% of the rated current; and 2) a RAMP\_TIME that is not excessively small.

Motors with larger inertia typically require smaller SFOC\_RAMP\_STEP and longer SFOC\_RAMP\_TIME.

For fast start-up with minimized start time, the ramp-up time in the open-loop state must be minimized. This may require an OL-CL transition frequency of less than 35 Hz at the expense of reliability. In addition, the value of RAMP\_STEP must be increased, the value of the current to start the motor must be increased to the value of 80% to 100% of the nominal current, and the RAMP\_TIME value must be reduced.

Generally, fast start-up demands high current.

## DRIVE—DRIVE

In the drive state the motor spins using a sensorless field-oriented control (SFOC) technique.

In sensorless operation, the motor angle and speed are estimated based on the motor electrical model (inductance, resistance) and the voltage and current that are applied.

In the drive state, the current can be further controlled and limited by the following parameters:

- SFOC\_DRV\_CURR\_DRV\_LMT sets the maximum current driving capability of the Q axis.
- SFOC\_DRV\_CURR\_RATE\_LMT and SFOC\_DWN\_CURR\_RATE\_LIMIT limit the rate of growth and decrease of the current on the Q axis.

To prevent sudden changes in the torque applied to the motor, which could result in acoustic noise, the A89333-1 provides the option to limit the maximum rate of change of the speed command by using the SFOC\_REF\_RATE\_LMT parameter.

## REGENERATIVE MODE

In case of strong deceleration, the motor can operate as a generator and transfer energy back to the power. If the power supply is not able to absorb the energy,  $V_{BB}$  voltage is increased [pumped up; PUP], with the potential to damage the system.

The A89333-1 can limit the  $V_{BB}$  pump-up using the SFOC\_VBB\_LMT and SFOC\_VBB\_LMT\_TH parameters. Alternatively, the  $I_q$  regenerative current can be limited using the SFOC\_CURR\_GEN\_LMT and SFOC\_GEN\_CURR\_RATE\_LMT parameters.

## BRAKE—BRAKE

Brake mode enables rapid motor shutdown, when desired. During braking, the three low-side drivers—connecting the three motor terminals together and short the motor BEMF—are enabled. In brake mode, the current of the winding is limited only by the motor and the resistance of the external FETs. Because of this, care must be taken to avoid excessive current in the FETs when braking. Several configuration options are available for programming in the NVM to allow for safe braking, such as pulsed braking and braking hold-off based on motor frequency.

In the brake state, the device activates the low-side MOSFET, braking the motor according to these parameters:

- BRAKE\_FET\_ON\_DURATION
- BRAKE\_FET\_OFF\_DURATION

If motor speed exceeds BRAKE\_FREQ\_TOO\_HIGH\_TH, the motor coasts before the brake is activated. This prevents generation of excessively high current that could damage the MOSFET or the motor.

The device enters the brake state when one of these conditions is verified:

- Pin nBRAKE is driven low.
- Brake bit is set in the BRAKE\_CTRL register.
- Windmill state is active and a braking feature is required, as described in the Windmilling—WNDML section.
- Speed command MCA\_COMMAND is less than CMD\_OFF\_TH and BRAKE\_IF\_OFF\_EN = 1. If BRAKE\_IF\_OFF\_EN = 0, the device enters the standby state and the motor coasts.

If BRAKE\_IF\_OFF\_EN = 1, the device also keeps the motor braked (low-side MOSFET on) after the motor stops.

NOTE: If SOFT\_OFF\_EN is set, the motor can be decelerated in the closed-loop state (drive state). For more information about soft deceleration of the motor, refer to the [APEK89333 user manual](#)<sup>[1]</sup> available on the Allegro website.

## FOC Algorithm Speed and Current Loop

In speed mode, the command from MCA\_COMMAND is used as a reference set point to the speed loop, and the output of the speed loop is used as the reference for the Q-axis current in the current loop.

In torque mode, the command from MCA\_COMMAND is passed directly to the current loop as the reference for the Q-axis current.

[1] [https://www.allegromicro.com/-/media/files/demo-boards/user-manuals/apex89333-eval-board-user-manual.pdf?sc\\_lang=en](https://www.allegromicro.com/-/media/files/demo-boards/user-manuals/apex89333-eval-board-user-manual.pdf?sc_lang=en)

The reference for the D-axis current can be set using the register SFOC\_DRV\_D\_CURR\_REF; however—to ensure that the stator and rotor field are 90° out of phase with each other, which allows for the maximum available torque and system efficiency—the recommended setting is zero.

PI controllers, one for speed and one for current loop, can be tuned using SFOC\_D\_CURR\_KP, SFOC\_D\_CURR\_KI, SFOC\_Q\_CURR\_KP, and SFOC\_Q\_CURR\_KI NVM settings.

The A89333-1 integrates a space-vector modulation (SVM) technique that optimizes use of the supply voltage and increases the base motor speed. The algorithm also implements a  $V_{BB}$  compensation feature that automatically adjusts the duty cycle to correct disturbances or sudden voltage variations on the supply voltage. The system works as a percentage of the nominal  $V_{BB}$  ( $VBB\_NOM$  NVM parameter) and calculates the duty cycle,  $\delta$ , for phase voltages according to:

Equation 12:

$$\delta = \frac{V_{phase}}{VBB_{measured}(\%) \times VBB_{nom}}$$

**Example 1:**

$VBB_{nom} = 12\text{ V}$

$v_{phase}$  calculated from FOC algorithm is 50% of  $VBB_{nom}$

$VBB_{measured}$  from ADC = 12 V, so it is 100% of  $VBB_{nom}$

Calculation of  $\delta$ :

Equation 13:

$$\begin{aligned} \delta &= \frac{V_{phase}}{VBB_{measured}(\%) \times VBB_{nom}} \\ &= \frac{50\% VBB_{nom}}{100\% \times VBB_{nom}} \\ &= 50\% \end{aligned}$$

**Example 2:**

$VBB_{nom} = 12\text{ V}$

$v_{phase}$  calculated from FOC algorithm is 50% of  $VBB_{nom}$

$VBB_{measured}$  from ADC = 6 V, so it is 50% of  $VBB_{nom}$

Calculation of  $\delta$ :

Equation 14:

$$\begin{aligned} \delta &= \frac{V_{phase}}{VBB_{measured}(\%) \times VBB_{nom}} \\ &= \frac{50\% VBB_{nom}}{50\% \times VBB_{nom}} \\ &= 100\% \end{aligned}$$

The compensation of  $V_{BB}$  is guaranteed until  $V_{BB}$  measured is less than  $2 \times VBB_{nom}$ .

## OBSERVER

For sensorless-mode operation, the motor angle and speed data are estimated in the observer block—without the need for an external sensor.

The machine parameters required in the A89333-1 observer are the motor phase inductance,  $sfocLs$ , and the motor phase resistance,  $sfocRs$ , according to:

Equation 15:

$$sfocLs = round \left( \frac{2\pi \times i_{max} \times f_{res} \times motorLs \times 2^{(sfocLsFl+21)}}{0.298 \times VBB_{nom}} \right),$$

where:

- $sfocLs$  [unitless] is the stator inductance NVM setting.
- $i_{max}$  [A] is the maximum system current.
- $f_{res} = \frac{1}{9 \times 2^{sfocFreqRes}}$  [Hz/LSB] is the frequency resolution.
- $motorLs$  [H] is the motor phase to neutral inductance (phase-to-phase/2).
- $sfocLsFl$  [unitless] is the SFOC stator inductance fractional length NVM setting (signed).
- $VBB_{nom}$  [V] is the nominal DC link voltage (should be in alignment with the  $VBB_{nom}$  setting).

Equation 16:

$$sfocRs = round \left( \frac{motorRs \times i_{max} \times 2^{(sfocRsFl+11)}}{0.298 \times VBB_{nom}} \right),$$

where:

- $sfocRs$  [unitless] is the stator resistance NVM setting.
- $i_{max}$  [A] is the maximum system current.
- $motorRs$  [ $\Omega$ ] is the motor phase to neutral resistance (phase-to-phase/2).
- $sfocRsFl$  [unitless] is the SFOC stator inductance fractional length NVM setting (signed).
- $VBB_{nom}$  [V] is the nominal DC link voltage (should be in alignment with  $VBB\_NOM$  setting).

Proper functioning of the observer requires proper tuning of the controller parameters SFOC\_PO\_FREQ\_K and SFOC\_PO\_THETA\_K.

## DIAGNOSTIC AND PROTECTION FEATURES

A89333-1 integrates advanced diagnostics for critical hardware protection and motor control diagnostics. Hardware protections include overvoltage, undervoltage, over temperature, and short-circuit protection. Motor control diagnostics include lock detection (loss of sync) and no-motor start.

If a fault event occurs, the nFLT pin is pulled low to indicate a fault condition. The nFLT pin can also be connected to the nBRAKE pin to brake the motor in case of an overcurrent fault. Braking is not allowed for the OVP, UV, OT, and lock detection states.

Every fault can be enabled or disabled (masked) using the NVM parameters UVS\_DISABLE, OVT\_DISABLE, OVP\_ENABLE, OCP\_ENABLE, ROT\_STALL\_DET\_CTR = 0, and NO\_MOTOR\_START\_EN.

Fault data flags can be read in the SW status register via I<sup>2</sup>C communication.

**Table 4: Fault Table**

Fault	Fault Action	Latched
V <sub>BB</sub> Undervoltage	Disable outputs	N
Over Temp. Protection	Disable outputs	N
V <sub>BB</sub> Overvoltage Protection (V <sub>BB</sub> OVP)	Disable outputs	N
Overcurrent Protection (OCP)	Disable outputs Latch reset with command off/ on sequence or power-cycle	Y
Loss of Sync (Lock Det)	Set lock detect timeout— disable outputs	(SW latched fault)
No-Motor Start	Set lock detect timeout— disable outputs	(SW latched fault)

### V<sub>BB</sub> UNDERVOLTAGE—V<sub>BB</sub> UVS

When digital logic is running and the supply voltage on the V<sub>BB</sub> pin reduces to less than the UVS\_TH, the A89333-1 disables the outputs until the supply voltage reduces to less than the operating threshold, which is lower than the V<sub>BBUVLO</sub> threshold.

After the V<sub>BB</sub> undervoltage is detected, the outputs are disabled, the controller enters the fail mode, and fault reporting is performed by pulling low the nFLT pin and setting the corresponding fault flag in the SW status register. When the V<sub>BB</sub> level rises to greater than UVS\_TH (plus the hysteresis level), the outputs are re-enabled automatically (not latched), the fault flag is cleared, and the controller transitions to the standby mode and state. In the standby state, the controller verifies that the command exceeds the threshold of CMD\_ON\_TH, then transitions to

the windmill state, where a speed check is performed and used by the device to determine if the start is from a stationary position or with a moving rotor.

The V<sub>BB</sub> undervoltage protection level is programmable in NVM using the UVS\_TH parameter (see Table 5). The V<sub>BB</sub> undervoltage diagnostic is independently activated by the control method and state. If needed, the fault can be masked using the UVS\_DISABLE parameter in NVM.

**Table 5: UVS\_TH Parameter**

UVS_TH	V <sub>BB</sub> UVS (V)
0	32
1	25
2	7

### V<sub>BB</sub>, UV, AND NVM REPROGRAMMING

When the device is in an undervoltage (UV) state but the V<sub>BB</sub> exceeds the operating threshold of the supply voltage for digital logic, if in user mode, it is possible to reprogram the NVM (EEPROM) registers regardless of the selected external command source and the state of the FG pin. Changes to NVM take effect only after POR.

The UV condition prevents incorrect transactions that can result from FG/RD pin toggling and guarantees that the FG/RD pin is in the proper state for I<sup>2</sup>C for any NVM configuration. To program the EEPROM, increase V<sub>BB</sub> beyond 25 V after I<sup>2</sup>C communication is established.

If the FG/RD pin configuration cannot cause toggling (FG/RD pin is in the high state), it is possible to use I<sup>2</sup>C without UV and the EXT\_CMD\_SRC is not I<sup>2</sup>C. This allows NVM shadow programming when in user mode or SW status register consultation for diagnostic purposes. In this case, serial communication should be performed when the controller is in the standby state (motor stopped), and it can lead to unexpected motor starts.

### OVERTEMPERATURE PROTECTION—OVT/TSD

The A89333-1 protects itself from overheating with an internal thermal monitoring circuit. If the junction temperature exceeds the upper threshold T<sub>J\_TSD</sub>, when the OVT is detected, the outputs are disabled, the controller enters the fail mode, and fault reporting is performed by pulling low the nFLT pin and setting the corresponding fault flag in the SW status register.

When device temperature returns to less than the T<sub>J\_TSD</sub> threshold minus the hysteresis level, ΔT<sub>J</sub>, the outputs are re-enabled automatically (not latched), the fault flag is cleared, and the controller transitions to the standby mode and state. In the standby state, the controller verifies that the command exceeds the threshold of CMD\_ON\_TH, then transitions to the windmill state, where a

speed check is performed and used for the device to determine if the start is from a stationary position or with a moving rotor.

The over-temperature protection diagnostic is independently activated by the control method and state. If not needed, the fault can be masked using the OVT\_DISABLE parameter in NVM.

## OVERCURRENT PROTECTION—OCP (SHORT PROTECTION)

Overcurrent protection is intended to protect the power FETs from application conditions of shorted load, motor short to ground, and motor short to battery that can damage the system.

The  $V_{DS}$  voltages across each power MOSFET are monitored by the A89333-1. If any  $V_{DS}$  exceeds a predefined threshold (OCP\_TH), when the corresponding MOSFET is in the conduction mode (turned ON), an OCP fault is triggered and the output becomes disabled.

OCP_TH	$V_{DS}$ Threshold (V)
0	0.5
1	0.75
2	1.0
3	1.5

The  $V_{DS}$  threshold needs to be set as a function of the MOSFET ( $R_{DS(ON)}$ ) and to the maximum current that can be driven.

In case of a fault, the nFLT pin is pulled low, the fault flag is set in the SW status registers, and the output motor coasts (output disabled) or brakes using the low-side FETs (if the nFLT pin is connected to the nBRAKE pin). After braking completes (command off received; command is less than CMD\_OFF\_TH), a restart can be performed.

If braking is not configured, the bridge remains off and the restart procedure can be performed after the off command (the command is less than CMD\_OFF\_TH) is received.

Overcurrent protection (OCP) is a latched event and the output remains off until an off/on cycle command is received or the device is power-cycled.

OCP is independently activated by the control method and state. If not needed, the fault can be masked using the OCP\_ENABLE parameter in NVM.

## LOSS OF SYNC (LOCK/STALL DETECTION)

A89333-1 implements three stall detection mechanism selected by the ROT\_STALL\_DET\_CTRL parameter in NVM:

- Frequency estimation: The rotation frequency estimated by the observer,  $f_{est}$ , is compared to the predefined threshold configured in the ROT\_STALL\_TOO\_LOW\_SPEED\_TH. When  $abs(f_{est}) < ROT\_STALL\_TOO\_LOW\_SPEED\_TH$ , the stall state is detected immediately.
- $V_q$  estimation: The estimated  $V_q$  is compared to a range defined by ROT\_STALL\_DET\_HIGH\_TH and ROT\_STALL\_DET\_LOW\_TH. If the estimated  $V_q < ROT\_STALL\_DET\_LOW\_TH$  or  $V_q > ROT\_STALL\_DET\_HIGH\_TH$  for a duration exceeding ROT\_STALL\_DET\_TIME\_TH, the stall state is detected. For this estimate, the values of the motor phase resistance (SFOC\_RS) and the motor BEMF constant (SFOC\_KE) must be set. The motor BEMF constant (SFOC\_KE) is set according to:

Equation 17:

$$sfocKe = round \left( \frac{2\pi \times f_{res} \times motorKe \times 2^{(4+(8+sfocKeFl))}}{0.298 \times VBB_{nom}} \right)$$

where:

- sfocKe [unitless] is the motor BEMF NVM setting.
- $i_{max}$  [A] is the maximum system current.
- $f_{res} = \frac{1}{9 \times 2^{sfocFreqRes}}$  [Hz/LSB] is the frequency resolution.
- motorKe [V/(rad/s)] is the motor BEMF constant.
- sfocKeFl [unitless] is the SFOC stator inductance fractional length NVM setting (signed).
- $VBB_{nom}$  is the nominal DC link voltage (should be in alignment with the VBBNOM setting).
- BEMF estimation: The estimated BEMF is compared to the predefined threshold in ROT\_STALL\_TOO\_LOW\_V\_BEMF\_TH. If  $abs(bemf) < abs(threshold)$ , the stall state is detected immediately. The greater the value of ROT\_STALL\_TOO\_LOW\_VBEMF\_TH, the faster the BEMF stall detection feature will detect the stall; however, the chances of a false stall detection increase.

After the first rotor stall is detected, the outputs are disabled, the controller enters the fail mode, and the fault is reported, pulling low the nFLT pin and setting the corresponding

fault flag in the SW status register. The controller remains in the fail mode until the stall condition is absent, including during retries. Once the rotor is stalled, the controller tries to restart the motor for a total number of attempts set by ROT\_START\_RETRY\_MAX\_ATTEMPTS, with a delay of ROT\_STALL\_RETRY\_T\_OUT between each retry.

If the rotor is no longer in the stall state during the retries, the outputs are re-enabled automatically, the fault flag is cleared (not latched), and the controller transitions to the standby mode and state. In the standby state, the controller verifies that the command exceeds the threshold of the CMD\_ON\_TH parameter, then transitions to the windmill state, where a speed check is performed and used by the device to determine if the start is from a stationary position or with a moving rotor.

Alternatively, after the retry attempts complete, if the motor is still stalled, the controller checks if  $\text{command} < \text{CMD\_OFF\_TH}$  and, if not, remains in the fail mode and the standby state with the RS flag in the SW status register set. Otherwise, the fault and flag are cleared, and the MCA mode is changed to standby mode.

NOTE: Stall detection is masked during the open-loop (ramp-up) state and starts working only after the controller transitions to the closed-loop (drive) operation and ROT\_STALL\_BLANK\_DUR elapses.

## NO-MOTOR START

The no-motor start diagnostic detects a fault when a command to start the motor is applied without the motor connected to the board. The fault handling mechanism is the same as the stall detection fault.

## VBB OVERVOLTAGE VARIABLE LIMITER

If enabled (OVVL\_ENABLE), A89333-1 enters the OVVL condition when the voltage increases to greater than OVVL\_VOLT\_TH and it exits the condition when the voltage reduces to less than OVVL\_VOLT\_TH.

If the voltage increases to greater than OVVL\_VOLT\_TH, the

command is overwritten by the OVVL\_VAR\_LMT value. This prevents a further increase in voltage and does not trigger any faults.

Overvoltage detection is not considered a fault, and it greatly influences the maximum power limit function.

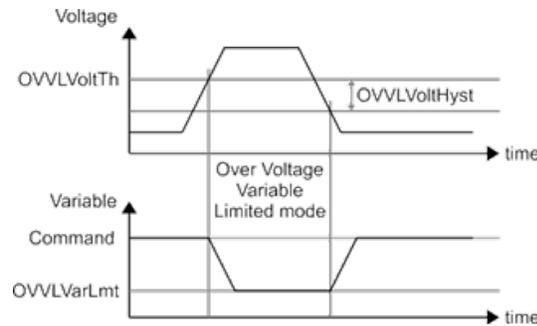


Figure 13: OVVL Timing Diagram

## OVERCURRENT LIMIT

A89333-1 can limit the maximum Q-axis current setting using the SFOC\_DRV\_CURR\_DRV\_LMT parameter in NVM as a percentage of the maximum current ( $I_{\max}$ ) that the system can handle. The Q-axis current limit is also designed to avoid demagnetization of permanent magnets. This is not considered a fault.

## MAXIMUM POWER LIMIT

By monitoring  $V_{BB}$  and  $I_{BB}$ , the A89333-1 reduces the output current when the maximum power limit is exceeded and regulates the power around the NVM-programmed maximum power limit (SFOC\_PWR\_LMT). The maximum power limit can be applied in all control modes: speed, torque, and power. This limit is set as a percentage of the maximum power ( $P_{\max}$ ) that the system can manage. For details, refer to the APEK89333 user manual available on the Allegro website.

## APPLICATION FEATURES

### EEPROM NVM for Storing Motor Control and Configuration Data

Motor control and configuration data are user-programmable and stored in the EEPROM of the IC.

Upon power-up, the A89333-1 waits for the internal regulators to reach their UVLO levels, then loads the configuration data from the EEPROM. After the configuration is loaded, the A89333-1 is in standby mode and is ready to respond to user input through the PWM/SPD pin or I<sup>2</sup>C port. The A89333-1 power-up and initialization sequence is shown in Figure 14.

### FG/RD Pin

A89333-1 FG/RD pin can be configured in the four states described in this section.

### FG

When EN\_FG\_FUNC is set, a square wave representing the electrical rotation frequency is generated on the FG/RD pin to attain the motor speed according to:

- If FG\_PP = 0 (NVM parameter) is selected:

Equation 18:

$$FG_{freq}[Hz] = 0.00390625 \times (FG_{gain} + 1) \times f_{elect}[Hz].$$

- If FG\_PP = 1...7 (NVM parameter) is selected:

Equation 19:

$$FG_{freq}[Hz] = \frac{0.00390625 \times (FG_{gain} + 1)}{FG_{pp} + 1} \times f_{elect}[Hz],$$

where FG<sub>gain</sub> is an NVM parameter that can assume integer values between 0 and 1023.

Typical configuration is to set FG\_GAIN = 255 and FG\_PP to number of motor pole-pairs. With such a configuration, the FG pin toggles with electrical frequency normalized to pp/2.

According to FG\_START\_TYPE, the FG signal can be generated once FOC starts, during ramp-up or after rotor synchronization (drive state).

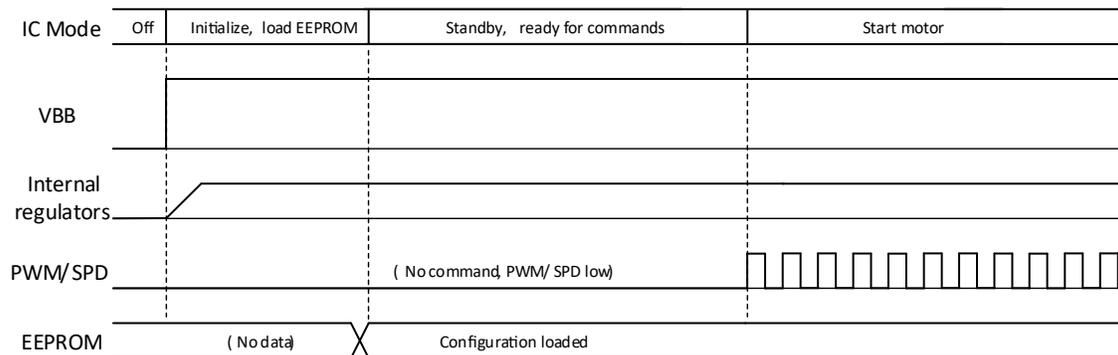


Figure 14: Power-Up and Initialization Sequence

## RD

When the RD feature is enabled (EN\_RD\_FUNC), the stalled condition is reported on the FG/RD pin according to the RD\_ACTIVE\_LEVEL parameter in NVM:

- RD\_ACTIVE\_LEVEL = 0: If a stall condition occurs, the FG/RD pin is set high.
- RD\_ACTIVE\_LEVEL = 1: If a stall condition occurs, the FG/RD pin is set low.

The pin remains in the active level throughout the duration of the presence of the stalled latch.

## FG IN VBB UV CONDITION

Because the FG pin shares the SDA pin of the I<sup>2</sup>C serial communication, if an undervoltage fault is present, the FG pin is set to a high (logic 1) state, enabling I<sup>2</sup>C communication. For more information, refer to the VBB, UV, and NVM Reprogramming section. During this fault, the pin is set to logic 1, and the FG ID pattern generation stops. After V<sub>BB</sub> voltage increases to greater than the undervoltage threshold, the FG pin is set to the default state and, if the EN\_FG\_ID parameter is set, FG ID is reinitialized and generated. This is the only option that allows the FG ID pattern to be generated more than once in a power cycle.

## FG ID PATTERN GENERATION

If FG ID pattern generation (EN\_FG\_ID) is set, a programmable identification clock signal is provided on the FG/RD pin upon startup so that a particular fan system can be identified. Upon power-up, the SPD/PWM pin must be low. During this state, the ID clock is available for a programmable duration from 1.125 s to 9 s, with resolution of 1.125 s or until the SPD/PWM pin remains low.

The ID clock frequency (FG\_ID\_FREQ) and duration (FG\_ID\_DUR) are configurable in NVM.

Frequency is calculated by:

Equation 20:

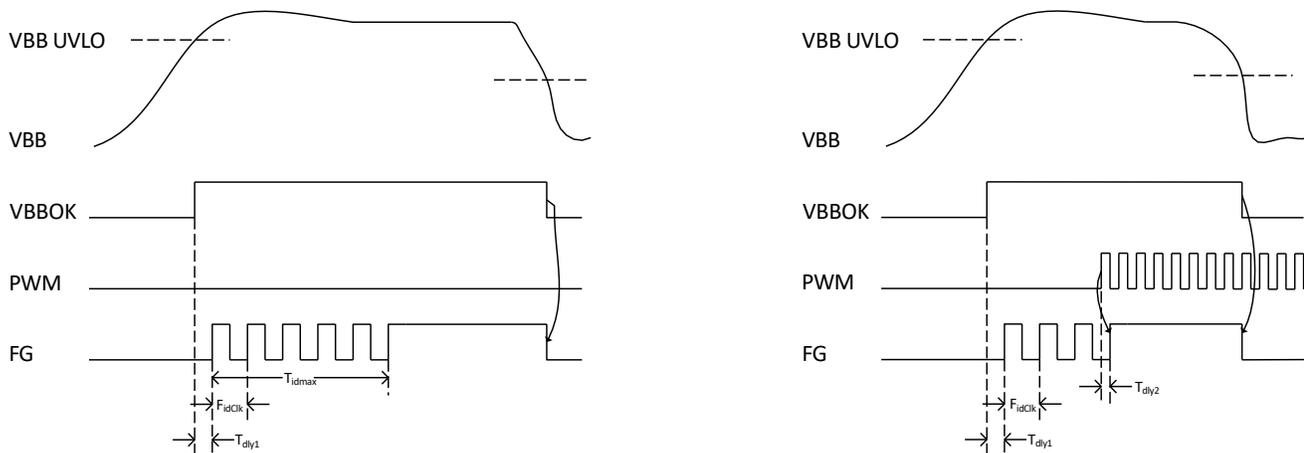
$$f_{FGID} = 266.7 + FGIDFreq \times 8.9 \text{ [Hz]} .$$

Duration is calculated by:

Equation 21:

$$t_{FGID} = (FGIDDur + 1) \times 1.125 \text{ [s]} .$$

If configured, the FG ID pattern is generated once per power cycle, after POR; and it is stopped if it reaches its duration, the command above threshold (CMD\_ON\_TH), or if the undervoltage fault is present.



$$T_{dly1} = 1/(2 \times F_{idClk}) + 0.001; T_{dly2} = 1/(2 \times F_{idClk})$$

Figure 15: ID Clock



## Advanced Features

### BEMF COMPENSATION

The A89333-1 implements a BEMF compensation function to improve acoustic performance and control efficiency. This feature is suitable for motors with strong cogging that do not have a pure sinusoidal BEMF and therefore could generate side harmonics when the pure sinusoidal voltages of the FOC algorithm are applied.

The presence of a noncompensated harmonic in the BEMF produces a significant ripple in current, which leads to energy wasted in the process of trying to demagnetize the permanent magnet and torque ripple that causes oscillation in the rotor and vibrations responsible of acoustic noise and damages in the ball bearings.

For more information about this advanced feature, refer to the APEK89333 user manual available on the Allegro website.

### SOFT-OFF DECELERATION

A89333-1 implements the soft-off deceleration feature, which allows selection of motor deceleration method before it stops. For more information about this advanced feature, refer to the APEK89333 user manual available on the Allegro website.

### SOFT START

Soft start allows for the quiet application of current before the align or ramp-up state: It avoids the onset of the inrush current, which is caused by the presence of current-scaling references required in the align and ramp-up states.

For more information about this advanced feature, refer to the APEK89333 user manual available on the Allegro website.

### QUIET START

To achieve a quieter OL-CL transition, A89333-1 implements a quiet start feature. The A89333-1 allows selection of a phase-current limit at the OL-CL transition.

Current can also be reduced in the ramp-up (SFOC\_RUP\_D\_CURR\_REF), toward the end of the open-loop ramp-up period, by properly configuring the OL-CL transition duration.

When the level of current is close to the level of current required by the feedback control, the transition noise may be able to be minimized.

For more information about this advanced feature, refer to the APEK89333 user manual available on the Allegro website.

### FORCED OL

The forced OL feature allows the A89333-1 to switch from speed control to power or torque control when the external command exceeds a configurable threshold. Above the selected threshold, the reference can be selected to reach a specific desired value of power or torque, or the power/torque reference can be calculated from the applied PWM duty cycle/I<sup>2</sup>C command.

For more information about this advanced feature, refer to the APEK89333 user manual available on the Allegro website.

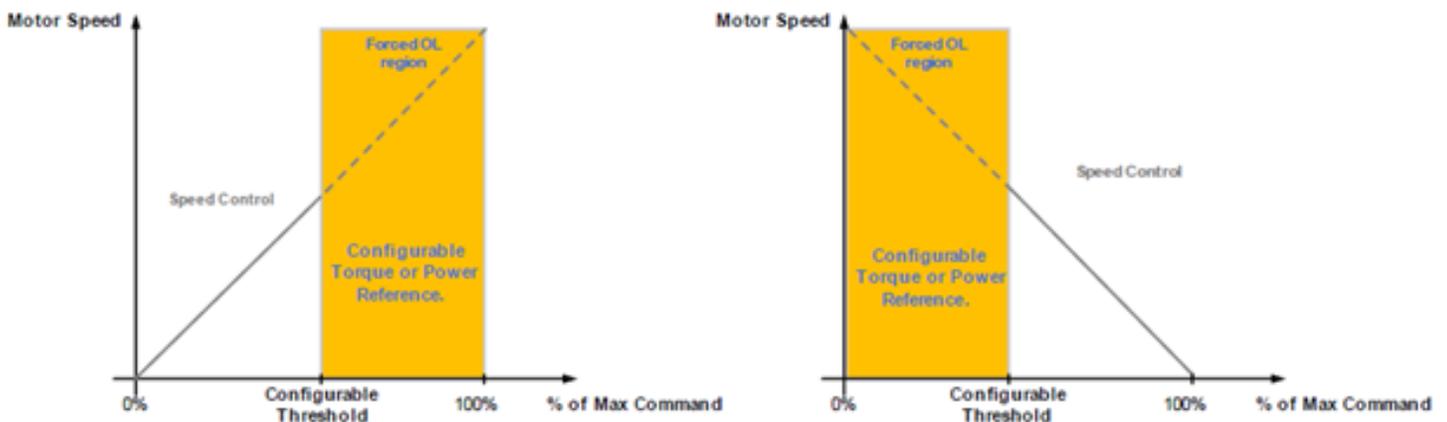


Figure 17: Forced OL High-Level Description

## VIN and Power-Loss Brake

The A89333-1 can detect a power loss by monitoring the VIN pin, and the brake function can be applied to slow the motor. When the motor spins, the BEMF voltage generated is rectified by the body diodes of the output DMOS devices and the V<sub>BB</sub> power supply capacitor is charged. If adequate voltage can be stored on the V<sub>BB</sub> capacitor, the low-side MOS devices can be turned on to provide braking force to the motor. When the motor slows, the generated BEMF voltage is reduced, eventually resulting in insufficient voltage on the V<sub>BB</sub> line to power the low-side MOSFETS; thus, the braking force is not applied and the motor coasts.

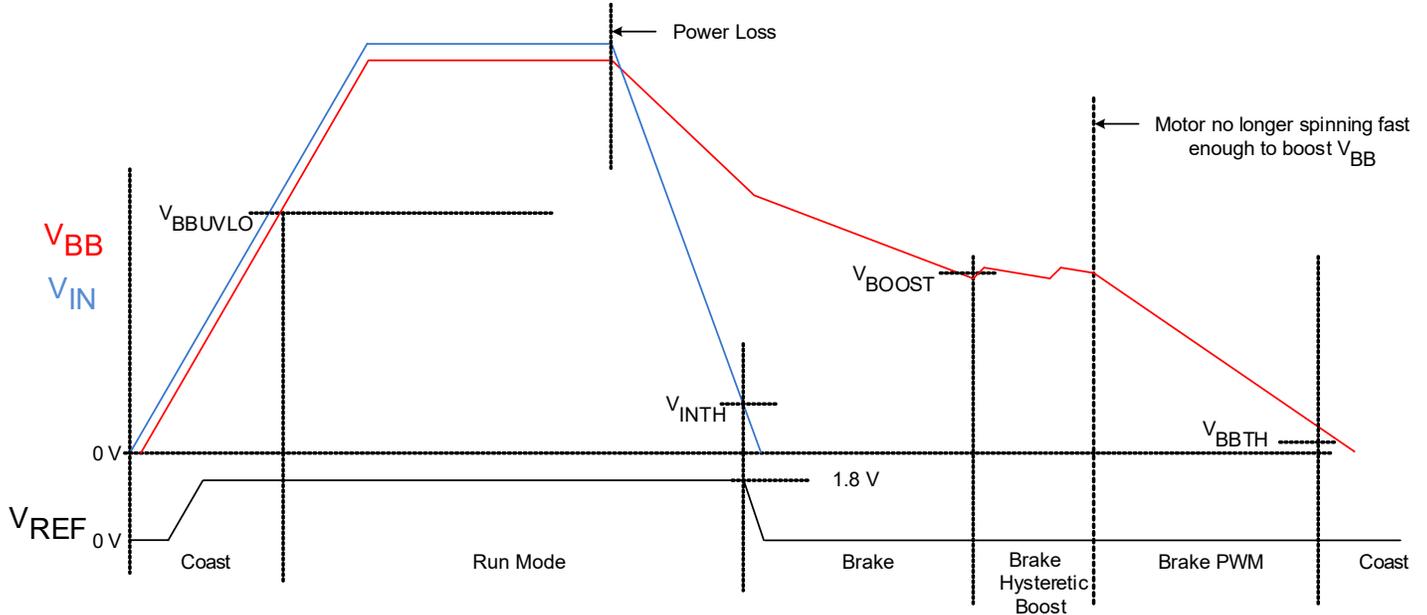
When the motor spins, the A89333-1 power-loss brake circuitry boosts the voltage on the V<sub>BB</sub> line by pulsing the motor windings off. If the motor is rotating, current is present in the motor winding when the brake is applied. This current can be used to charge up V<sub>BB</sub> capacitor and boost the V<sub>BB</sub> voltage by pulsing off the brake mode for a short time, similar to hysteretic boost converter operation. This, in turn, allows the IC to brake the motor at a much lower speed than otherwise possible.

Modes of operation depending on the state of the VBB and VIN pins are detailed in Table 6 and Figure 18.

**Table 6: Operation Modes Based on VBB and VIN Pin States**

VIN [1]	VBB	Mode of Operation	Notes
Low	< V <sub>BBTH</sub>	Coast—No braking	
Low	> V <sub>BBTH</sub> and < V <sub>BOOST</sub>	Brake PWM	If motor spin is sufficiently fast, V <sub>BB</sub> ramps up to V <sub>BOOST</sub>
Low	= V <sub>BOOST</sub>	Brake—Hysteretic boost	V <sub>BB</sub> is regulated to V <sub>BOOST</sub>
Low	> V <sub>BOOST</sub>	Brake	V <sub>BB</sub> decays depending on I <sub>BB2</sub> and V <sub>BB</sub> capacitance
High	< V <sub>BBUVLO</sub>	Coast—No braking	Power-up or power-down
High	> V <sub>BBUVLO</sub>	Run	V <sub>REF</sub> powers up logic; motor starts if PWM signal is valid

[1] V<sub>IN</sub> < V<sub>INTH</sub> = Low; V<sub>IN</sub> > V<sub>INTH</sub> = High

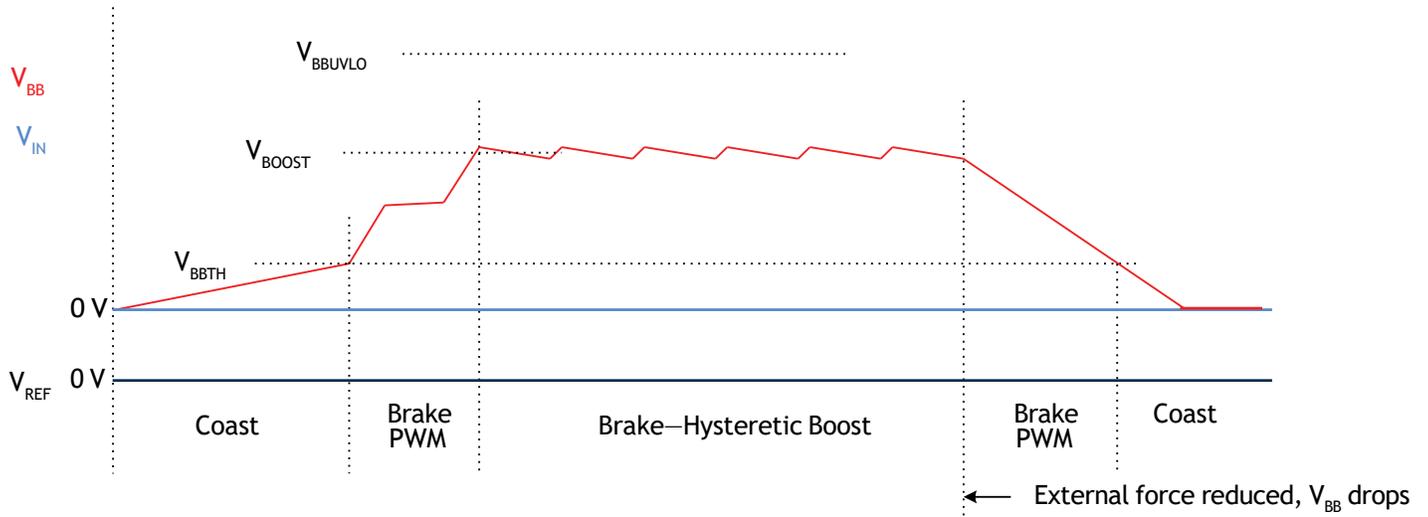


**Figure 18: Typical Power-Up and Power-Loss Sequence**

## No-Power Brake

Braking is also possible when power is not supplied to the module and the motor is spun by external force (i.e., windmill situation), as shown in Figure 17. In this case, the generated BEMF voltage increases  $V_{BB}$  beyond the  $V_{BBTH}$ , which enables the braking process.

For more information, refer to the APEK89333 user manual available on the Allegro website.



**Figure 19: Motor Spinning By External Force, Power Not Applied to Fan Module**

## REGISTERS AND NONVOLATILE MEMORY (NVM) MAP

A89333-1 uses NVM to store configuration data. Configuration data can be adjusted for a particular application. Upon power-up, the contents of the NVM are copied into registers (often called shadow registers) before they can be accessed by the logic circuits and used to control the motor operation. Direct access to shadow registers is also allowed through I<sup>2</sup>C interface. Writing to the shadow registers typically changes the operation of the driver immediately. (Some settings, the A89333-1 must enter standby mode, and the motor must be restarted before changes take effect). Changes made to NVM do not affect device operation until power is cycled.

I <sup>2</sup> C EEPROM NVM Register (Hex)	I <sup>2</sup> C Shadow Register (Hex)	EE Address (Hex)	NVM	Bits	Name	Value (Dec)	Default	Description
4C0	460	0	0	2:0	WNDML_MAX_ERR_ATTEMPTS	[0:7]	0x0	Maximum number of errors before exit to windmill error state (N + 1)
				5:3	WNDML_MAX_TO_ATTEMPTS	[0:7]	0x0	Maximum number of timeouts before rotor is considered to be stationary (N + 1)
				8:6	WNDML_NUMBER_OF_ASSESSMENTS	[0:7]	0x0	Quantity of windmill assessments to perform (N + 1)
				9	WNDML_TIMER_PRESCALER	[0:1]	0x0	Windmill timer prescaler: $t_{\text{tick}} = (1 + \text{TIMER\_PRESCALER}) \times t_{\text{clk}}$
				12:10	WNDML_TIMEOUT_PERIOD	[0:7]	0x0	Windmill timeout (1/2 of rotor period): For $\text{WNDML\_TIMER\_PRESCALER} = 0$ (frequency range 3000 Hz to 2 Hz): 0 = 20 ms 1 = 40 ms 2 = 81 ms 3 = 121 ms 4 = 162 ms 5 = 202 ms 6 = 243 ms 7 = 562 ms For $\text{WNDML\_TIMER\_PRESCALER} = 1$ (frequency range 750 Hz to 0.5 Hz): x2
				18:14	WNDML_EDGE_GLITCH_TIME	[0:31]	0x0	Edge glitch blanking time $(N + 1) \times 135 \times (\text{WNDML\_TIMER\_PRESCALER} + 1) \times t_{\text{clk}}$
				21:19	WNDML_DEBOUNCE_TICK	[0:7]	0x0	Debounce tick: 0 = 40 ns 1 = 1 $\mu$ s 2 = 11 $\mu$ s 3 = 115 $\mu$ s 4 = 1.1 ms 5 = reserved 6 = reserved 7 = reserved
				26:22	WNDML_DEBOUNCE_DELAY	[0:31]	0x0	Debounce time in debounce tick: $2^N$
31:27	SFOC_REF_RATE_LIMIT	[0:31]	0x0	Reference rate limit, $[0.09312u\% \times 2^N]$ of maximum (system) speed per VCL update				

I <sup>2</sup> C EEPROM NVM Register (Hex)	I <sup>2</sup> C Shadow Register (Hex)	EE Address (Hex)	NVM	Bits	Name	Value (Dec)	Default	Description
4C1	461	1	1	4:2	IPD_MAX_ERR_ATTEMPTS	[0:7]	0x0	maximum number of errors before return of error code, for Stage 1 and Stage 2
				7:5	IPD_NMBR_OF_EXCIT_ELEMENTS	[0:7]	0x0	Number of Stage 1 Base excitation elements to perform
				10:8	IPD_PWM_PERIOD	[0:7]	0x0	Duration of PWM period for IPD; 0 - 750 clk (33.33 kHz): 1 = 875 clk (28.57 kHz) 2 = 1000 clk (25 kHz) 3 = 1125 clk (22.22 kHz) 4 = 1250 clk (20 kHz) 5 = 1375 clk (18.18 kHz) 6 = 1500 clk (16.67 kHz) 7 = 1625 clk (15.38 kHz)
				12:11	IPD_STG1_ROUND_PAUSE	[0:3]	0x0	Pause after rounds of stage 1: 0 = 18 µs 1 = 36 µs 2 = 72 µs 3 = 144 µs
				13	IPD_STG2_CSA_GAIN	[0:1]	0x0	IPD stage 2, current sense amplifier (CAS) gain: 0 = 20 V/V 1 = 10 V/V
				14	IPD_STG2_TYPE	[0:1]	0x0	IPD stage 2 type: 0 = constant-current (IPD comparator) mode 1 = constant time (ADC current measurement) mode
				20:15	IPD_IPDDAC_CODE	[0:63]	0x0	Configuration of IPD DAC output signal for stage 2 of IPD: 2.4 V - N × 37.5 mV
				22:21	IPD_BLANKING_TIME	[0:3]	0x0	IPD comparator blanking time: 560 ns + (N × 2.88 µs)
				25:23	IPD_STG2_ROUND_PAUSE	[0:7]	0x0	Pause after rounds of stage 2: (2 <sup>N</sup> ) × 90 µs
				30:26	IPD_STG2_PULSE_DURATION	[0:31]	0x0	Stage 2 pulse duration [maximum value (timeout) in constant-current mode, pulse duration in constant time mode]: 0 = 14 µs 1 = 17 µs 2 = 22.5 µs 3 = 33.5 µs 4 = 45 µs 5 = 56 µs 6 = 67.5 µs 7 = 90 µs 8 = 112 µs 9 = 135 µs 10 = 225 µs 11 = 281 µs 12 = 394 µs 13 = 562 µs 14 = 843 µs 15 = 1.1 ms 16 = 2.2 ms 17 = 4.5 ms 18:31 = reserved
31	IPD_STG2_SATURATION_TH	[0:1]	0x0	Stage 2 measurement equality threshold: 0 = 3.125% 1 = 6.25%				

I <sup>2</sup> C EEPROM NVM Register (Hex)	I <sup>2</sup> C Shadow Register (Hex)	EE Address (Hex)	NVM	Bits	Name	Value (Dec)	Default	Description
4C2	462	2	2	7:0	PWM_PERIOD	[0:255]	0x0	PWM period duration: $(N \times 16 + 800) \times t_{clk}$
				15:8	PWM_DEAD_TIME	[0:255]	0x0	PWM dead time pause duration: $N \times t_{clk}$
				17:16	RESERVED	[0:3]	0x0	Reserved
				20:18	RESERVED	[0:7]	0x0	Reserved
				21	PWM_HIGH_RES	[0:1]	0x0	PWM high-resolution mode: 1 = enable 0 = disable
				23:22	PWM_REFRESH_PERIODICITY	[0:3]	0x0	Periodicity of bootstrap refresh pulse insertion, PWM periods: 0 = 4th PWM period 1 = 6th PWM period 2 = 8th PWM period 3 = 10th PWM period
				26:24	PWM_REFRESH_PULSE_DURATION	[0:7]	0x0	Bootstrap refresh pulse duration, $N \times t_{clk}$ : 0 = off 1 = 12 (0.48 $\mu$ s) 2 = 23 (0.92 $\mu$ s) 3 = 34 (1.36 $\mu$ s) 4 = 68 (2.72 $\mu$ s) 5 = 101 (4 $\mu$ s) 6 = 141 (5.6 $\mu$ s) 7 = 197 (7.9 $\mu$ s)
				29:27	PWM_REFRESH_THRESHOLD	[0:7]	0x0	Bootstrap refresh threshold, duty cycle that enables bootstrap refresh feature, % of PWM period: 0 = 100% 1 = 99.21875% 2 = 98.4375% 3 = 97.65625% 4 = 96.875% 5 = 96.09375% 6 = 95.3125% 7 = 94.53125%
31:30	PWM_GD_SLEW_RATE	[0:3]	0x0	Gate driver slew current setting, four settings: 0 = 10 mA for HS, 30 mA for LS 1 = 30 mA for HS, 50 mA for LS 2 = 50 mA for HS, 70 mA for LS 3 = 70 mA for HS, 70 mA for LS				
4C3	463	3	3	0	SFOC_CSA_GAIN	[0:1]	0x0	SFOC CSA (current sense amplifier) gain: 0 = 20 V/V 1 = 10 V/V
				3:1	SFOC_VCL_UPDATE_RATE	[0:7]	0x0	SFOC VCL update rate in number of PWM periods: $2^N$
				5:4	SFOC_FREQUENCY_RES	[0:3]	0x0	SFOC frequency resolution: 0 = 0.111 Hz 1 = 0.056 Hz 2 = 0.028 Hz 3 = 0.014 Hz
				14:6	SFOC_RAMP_TIME	[0:511]	0x0	Ramp-up time: $[40 + 256 \times N]$ VCL updates
				24:15	SFOC_RAMP_STEP	[0:1023]	0x0	Ramp-up frequency (speed) rate: $[(N + 1) \times 0.0244140625]$ of maximum (system) speed per second
				31:25	SFOC_FREQUENCY_LMT	[0:127]	0x0	Speed limit: $(N + 1) \times 0.78125\%$ of maximum (system) speed
4C4	464	4	4	3:0	SFOC_BRAKE_ALGN_CONST_DQ_CURR_KP	[0:15]	0x0	Brake align constant D/Q current PI controller proportional gain (signed): $2^N$
				9:4	SFOC_BRAKE_ALGN_CONST_DQ_CURR_KI	[0:63]	0x0	Brake align constant D/Q current PI controller integral gain (signed): $2^N$
				12:10	SFOC_RD_OL_SPEED_TH	[0:7]	0x0	Reverse-drive open-loop speed threshold: $(N + 1) \times 0.390625\%$ of maximum (system) speed
				17:13	SFOC_RD_D_CURR_REF	[0:31]	0x0	Reverse-drive D current reference: $(N + 1) \times 3.125\%$ of maximum current
				27:18	FG_GAIN	[0:1023]	0x0	FG (frequency generation) gain, FG_PP: 0 = $0.00390625 \times (N + 1)$ 1:7 = $0.00390625 \times (N + 1) \times 2 / (FG\_PP + 1)$
				30:28	FG_PP	[0:7]	0x0	Number of pole-pairs: $(N + 1)$
				31	NO_MOTOR_START_EN	[0:1]	0x0	No-motor start detection enable: 0 = disabled 1 = enabled

I <sup>2</sup> C EEPROM NVM Register (Hex)	I <sup>2</sup> C Shadow Register (Hex)	EE Address (Hex)	NVM	Bits	Name	Value (Dec)	Default	Description
4C5	465	5	5	11:0	SFOC_LS	[0:4095]	0x0	Stator inductance constant, unitless
				15:12	SFOC_LS_FL	[0:15]	0x0	Stator inductance constant FL (signed), 5 + N
				25:21	SFOC_RUP_D_CURR_REF	[0:31]	0x0	Ramp-up D current reference; (N + 1) × 3.125% of maximum current
				29:26	SFOC_DRV_D_CURR_REF	[0:15]	0x0	Drive D current reference: -1 × (N × 1.5625)% of maximum current
4C6	466	6	6	4:0	SFOC_D_CURR_KP	[0:31]	0x0	D current PI controller proportional gain (signed), 2 <sup>N</sup>
				10:5	SFOC_D_CURR_KI	[0:63]	0x0	D current PI controller integral gain (signed), 2 <sup>N</sup>
				15:11	SFOC_Q_CURR_KP	[0:31]	0x0	Q current PI controller proportional gain (signed), 2 <sup>N</sup>
				21:16	SFOC_Q_CURR_KI	[0:63]	0x0	Q current PI controller integral gain (signed), 2 <sup>N</sup>
				27:22	SFOC_PO_THETA_K	[0:63]	0x0	Position observer theta gain (signed), 2 <sup>N</sup>
4C7	467	7	7	5:0	SFOC_PO_FREQ_K	[0:63]	0x0	Position observer frequency gain (signed), 2 <sup>N</sup>
				8:6	SFOC_PO_ERR_LMT	[0:7]	0x0	Position observer error limit, 2 <sup>N</sup>
				10:9	SFOC_VAR_CTRL_MODE	[0:3]	0x0	Variable control mode (variable select): 0 = speed control 1 = power control 2 = torque control 3 = reserved
				16:11	SFOC_VAR_KI	[0:63]	0x0	Variable control (speed/power) integral gain (signed), 2 <sup>N</sup>
				21:17	SFOC_VAR_KP	[0:31]	0x0	Variable control (speed/power) proportional gain (signed), 2 <sup>N</sup>
				24:22	BEMF_COMP_N	[0:7]	0x0	Number of BEMF harmonics to be compensated
				30:25	BEMF_COMP_PHASE	[0:63]	0x0	Phase shift of BEMF-compensating component (signed), N × 3.125% of system angle
4C8	468	8	8	8:5	SFOC_ALGN_DQ_CURR_KP	[0:15]	0x0	Align D/Q current PI controller proportional gain (signed), 2 <sup>N</sup>
				14:9	SFOC_ALGN_DQ_CURR_KI	[0:63]	0x0	Align D/Q current PI controller integral gain (signed), 2 <sup>N</sup>
				19:15	SFOC_DRV_CURR_DRV_LMT	[0:31]	0x0	Drive Q current limit: (N + 1) × 3.125% of maximum current
				25:20	SFOC_CURR_GEN_LMT	[0:63]	0x0	Generator (regenerative brake) Q current limit: N × 1.5625% of maximum current
				31:26	SFOC_VBB_LMT	[0:63]	0x0	Voltage limit: 100% + N × 0.78125% of nominal voltage
4C9	469	9	9	5:0	SFOC_VBB_LMT_TH	[0:63]	0x0	Voltage limit threshold (below voltage limit): (N + 1) × 0.78125% of nominal voltage
				11:6	SFOC_PWR_LMT	[0:63]	0x0	Power limit: N × 1.5625% of [(3/2) × ((maximum current) × 1.1547 × (nominal voltage)/2)]
				17:12	SFOC_FREQUENCY_LMT_TH	[0:63]	0x0	Speed limit threshold (below speed limit): (N + 1) × 0.78125% of speed limit
				21:18	SFOC_VAR_ERR_LMT	[0:15]	0x0	Variable error limit (speed or power): 2 <sup>N</sup>
				22	SFOC_ACDC_ALIGN_TYPE	[0:1]	0x0	AC/DC align type: 0 = DC align 1 = AC align
4CA	46A	10	10	4:0	SFOC_ALGN_D_CURR_REF	[0:31]	0x0	Align D current reference: (N + 1) × 3.125% of maximum current
				10:5	SFOC_ALGN_TIME	[0:63]	0x0	Align time: 2048 × (N + 1) VCL updates
				15:11	SFOC_BRAKE_ALGN_CONST_D_CURR_REF	[0:31]	0x0	Brake align constant D current reference; (N + 1) × 3.125% of maximum current
				20:16	DTC_GAIN	[0:31]	0x0	Dead time compensation (DTC) gain
				27:21	DTC_MAX_TIME	[0:127]	0x0	Dead time compensation (DTC) maximum compensation time, in units of 6.25%
				31:28	SFOC_DWN_CURR_RATE_LIMIT	[0:15]	0x0	Down current rate limit, [2 <sup>(N+1)</sup> × 0.745 μ%] of maximum current per VCL update

I <sup>2</sup> C EEPROM NVM Register (Hex)	I <sup>2</sup> C Shadow Register (Hex)	EE Address (Hex)	NVM	Bits	Name	Value (Dec)	Default	Description
4CB	46B	11	11	7:0	MSQ_CST	[0:255]	0x0	Measurement-sequencer current-measurement settling time: $N \times t_{clk}$
				9:8	EXT_CMD_SRC	[0:3]	0x0	External command source: 0 = I <sup>2</sup> C 1 = VCMD 2 = duty cycle (PWM) 3 = frequency (SPD)
				11	ALIGN_TYPE	[0:1]	0x0	Align type: 0 = align 1 = IPD
				12	IPD_FAIL_ACTION	[0:1]	0x0	IPD fail action: 0 = perform alignment 1 = start from 0 angle
				13	EN_RD_FUNC	[0:1]	0x0	Enable rotation detection (RD) functionality: 0 = disabled 1 = enabled
				14	EN_FG_FUNC	[0:1]	0x0	Enable frequency generation (FG) functionality: 0 = disabled 1 = enabled
				15	PWM_MOD_MODE	[0:1]	0x0	PWM switching pattern configuration: 0 = edge start with compensation 1 = edge start without compensation
				23:16	VBB_NOM	[0:255]	0x0	Nominal $V_{BB}$ voltage; $N \times 0.515625$ V
				26:24	SYSTEM_TIMER_UPDATE_RATE	[0:7]	0x0	System timer update rate: $N = 0.5, 1188 \text{ ms}/2^{(N \times 2)}$ $N = 6:7, 1.16 \text{ ms}$
				27	FG_START_TYPE	[0:1]	0x0	FG start type: 0 = after FOC starts 1 = after rotor synchronizes
				28	RD_ACTIVE_LEVEL	[0:1]	0x0	Set rotation detection (RD) active high/low: 0 = high 1 = low
30:29	CAT_DUR	[0:3]	0x0	Current acquisition time duration: 0 = $1/16 t_{PWM}$ 1 = $1/20 t_{PWM}$ 2 = $1/32 t_{PWM}$ 3 = $1/40 t_{PWM}$				

I <sup>2</sup> C EEPROM NVM Register (Hex)	I <sup>2</sup> C Shadow Register (Hex)	EE Address (Hex)	NVM	Bits	Name	Value (Dec)	Default	Description
4CC	46C	12	12	1	FORCED_OL_EN	[0:1]	0x0	Forced OL enable: 0 = disabled 1 = enabled
				2	FORCED_OL_MODE_SEL	[0:1]	0x0	Forced OL mode select: 0 = torque 1 = power
				5:3	FORCED_OL_HYST	[0:7]	0x0	Forced OL torque/power hysteresis; 0.78125 × N% of maximum command
				6	ROSC_EXT_DIS	[0:1]	0x0	Disconnects external resistor from base OSC block, and connects digital test/debug input buffer; typical application configuration is ROSC_EXT_DIS = 0 (enabled, base RCO fully operational)
				7	NBRAKE_IN_DIS	[0:1]	0x0	Disables brake request via pin functionality: 0 = enabled 1 = disabled
				8	IPUP_NFLT_DIS	[0:1]	0x0	Internal pull-up resistor on nFLT pin disable: 0 = enabled 1 = disabled
				9	IPUP_FGRD_DIS	[0:1]	0x0	Internal pull-up resistor on FG/RD pin disable: 0 = enabled 1 = disabled
				10	IPUP_PWMSPD_DIS	[0:1]	0x0	Internal pull-up resistor on PWM/SPD pin disable: 0 = enabled 1 = disabled
				11	IPUP_NBRAKE_DIS	[0:1]	0x0	Internal pull-up resistor on NBRAKE pin disable: 0 = enabled 1 = disabled
				12	IPUP_DIR_DIS	[0:1]	0x0	Internal pull-up resistor on DIR pin disable: 0 = enabled 1 = disabled
				13	IPUP_SCLSEL_DIS	[0:1]	0x0	Internal pull-up resistor on SCLSEL pin disable: 0 = enabled 1 = disabled
				16:14	RESERVED	[0:7]	0x0	Reserved
				17	RESERVED	[0:1]	0x0	Reserved
				18	EN_PWMSPD_FILT	[0:1]	0x0	PWM/SPD pin filter enable: 0 = disabled 1 = enabled
				20:19	OCP_BLANK_TIME	[0:3]	0x0	Overcurrent protection VDS comparator blanking time: (N + 1) × 800 ns
				22:21	OCP_TH	[0:3]	0x0	Overcurrent protection VDS comparator threshold: 0 = 0.5 V 1 = 0.75 V 2 = 1 V 3 = 1.5 V
				24:23	OCP_DEB_TIME	[0:3]	0x0	Overcurrent protection VDS comparator debounce time: 0 = 10 × t <sub>clk</sub> 1 = 18 × t <sub>clk</sub> 2 = 25 × t <sub>clk</sub> 3 = 32 × t <sub>clk</sub>
				25	OCP_ENABLE	[0:1]	0x0	Overcurrent protection enable: 0 = disabled 1 = enabled
				27:26	UVS_TH	[0:3]	0x0	Undervoltage shutdown threshold: 0 = 32 V 1 = 25 V 2 = 7 V
				28	UVS_DISABLE	[0:1]	0x0	Undervoltage shutdown disable: 0 = enabled 1 = disabled
				29	OVT_DISABLE	[0:1]	0x0	Overtemperature shutdown disable: 0 = enabled 1 = disabled
30	NO_DRIVE_TELEMETRY_DIS	[0:1]	0x0	Disable telemetry measurements when motor is not being driven: 0 = enabled 1 = disabled				
31	I <sup>2</sup> C_RESPONSE_MODE	[0:1]	0x0	I <sup>2</sup> C protocol response mode: 0 = in frame 1 = out of frame				

I <sup>2</sup> C EEPROM NVM Register (Hex)	I <sup>2</sup> C Shadow Register (Hex)	EE Address (Hex)	NVM	Bits	Name	Value (Dec)	Default	Description
4CD	46D	13	13	10:4	FORCED_OL_CMD_REF	[0:127]	0x0	Forced OL torque/power command: 0 = not applied 1..127 = $[25 + 0.5859375 \times (N + 1)]\%$ of maximum command
				16:11	FORCED_OL_TH	[0:63]	0x0	Forced OL torque/power threshold: Inversion disabled = $[50 + 0.78125 \times (N + 1)]\%$ of maximum command Inversion enabled = $[50 - 0.78125 \times (N + 1)]\%$ of maximum command
				20:17	ROT_STALL_TOO_LOW_VBEMF_TH	[0:15]	0x0	Stall detection BEMF low threshold: $(N + 1) \times 0.78125\%$ of $[1.1547 \times (\text{nominal voltage}/2) \times (I_q/\text{maximum current})]$
				23:21	ROT_STALL_DET_CTRL	[0:7]	0x0	Rotor stall detection control: 0th bit = $V_q$ estimate 1st bit = frequency estimate 2nd bit = BEMF  Rotor stall detection control settings: 0 = disabled 1:7 = combination of stall detection options
				25:24	ROT_STALL_BLANK_DUR	[0:3]	0x0	Rotor stall blanking time duration: $[(\text{rotor synchronization timeout})/2^N]$
				29:26	ROT_SYNC_TOUT	[0:15]	0x0	Rotor synchronization timeout, in amount of VCL updates: $2^{(N + 8)}$
				30	NFLT_DIS	[0:1]	0x0	Disables fault indication via pin functionality: 0 = enabled 1 = disabled
				31	NFLT_STARTUP_DIS	[0:1]	0x0	Pull nFLT to zero during startup: 0 = enable 1 = disable
4CE	46E	14	14	5:2	ROT_STALL_DET_TIME_TH	[0:15]	0x0	Rotor stall detection time threshold, in amount of VCL updates: $2^{(N + 6)}$
				8:6	ROT_STALL_DET_HIGH_TH	[0:7]	0x0	Rotor stall detection high threshold: $100\% + (N + 1) \times 12.5\%$
				11:9	ROT_STALL_DET_LOW_TH	[0:7]	0x0	Rotor stall detection low threshold: $(N + 1) \times 12.5\%$
				15:12	ROT_STALL_TOO_LOW_SPEED_TH	[0:15]	0x0	Rotor stall too low speed threshold: $(N + 1) \times 0.09765625\%$ of maximum (system) speed
				31:16	CUSTOMER_PASSWORD	[0:65535]	0x0	Customer EEPROM password, 16 bit: 0x0000 and 0xFFFF are invalid password options (used to disable password protection)
4CF	46F	15	15	11:0	SFOC_RS	[0:4095]	0x0	Stator resistance, unitless
				14:12	SFOC_RS_FL	[0:7]	0x0	Stator resistance FL (signed), $6 + N$
				27:16	SFOC_KE	[0:4095]	0x0	Motor electrical constant, unitless
				30:28	SFOC_KE_FL	[0:7]	0x0	Motor electrical constant FL (signed), $8 + N$
4D0	470	16	16	2:0	EXT_CMD_FILTER_TAU	[0:7]	0x0	External command filter time constant, $2^{(14 - N)}$ samples: 0 = disabled
				3	ROT_DIR_INVERT	[0:1]	0x0	Rotation direction inversion: 0 = no inversion 1 = inversion
				4	EXT_CMD_AVERAGE_EN	[0:1]	0x0	External command average enable: 0 = disabled 1 = enabled
				7:5	STAT_START_ADVANCE_ANGLE	[0:7]	0x0	Stationary-start rotor-advance angle: $N \times 5.625^\circ$
				8	EN_FG_ID	[0:1]	0x0	Enable FG ID feature
				11:9	FG_ID_DUR	[0:7]	0x0	FG ID sequence duration: $(N + 1) \times 1.125$ s
				17:12	FG_ID_FREQUENCY	[0:63]	0x0	FG ID sequence frequency: $(266.7 + N \times 8.89)$ Hz
				20:18	WNDML_START_ADVANCE_ANGLE	[0:7]	0x0	Windmill-start rotor-advance angle: $N \times 5.625^\circ$
				22:21	ALIGN_START_ANGLE	[0:3]	0x0	Align-start rotor angle: $N \times 16.875^\circ$
				23	BOOTSTRAP_PRECHARGE_DURATION	[0:1]	0x0	Duration of bootstrap precharge procedure performed before start from stationary position: 0 = 36 $\mu$ s 1 = 72 $\mu$ s
				31:24	SH11_COMP	[0:255]	0x0	Single-shunt I1 current compensation: $2 \times N$

I <sup>2</sup> C EEPROM NVM Register (Hex)	I <sup>2</sup> C Shadow Register (Hex)	EE Address (Hex)	NVM	Bits	Name	Value (Dec)	Default	Description
4D1	471	17	17	0	BRAKE_TYPE	[0:1]	0x0	Brake type: 0 = low-side FET 1 = constant current
				2	BRAKE_IN_REVERSE_TYPE	[0:1]	0x0	Brake in reverse type: 0 = FOC decelerate 1 = brake
				3	BRAKE_IN_WNDML_ALWAYS_EN	[0:1]	0x0	Brake in windmill always enable: 0 = disabled 1 = enabled
				4	BRAKE_IF_OFF_EN	[0:1]	0x0	Brake if off enable: 0 = disabled 1 = enabled
				7:5	BRAKE_SEQ_LENGTH	[0:7]	0x0	Brake sequence length: $2^{(N+1)} - 1$
				10:8	BRAKE_FET_PULSE_AMOUNT	[0:7]	0x0	Brake by FET pulses amount: $2^{(N+1)}$
				13:11	BRAKE_FET_ON_DURATION	[0:7]	0x0	Brake by FET on duration: $(2^N) \times 11.24 \mu\text{s}$
				15:14	BRAKE_FET_OFF_DURATION	[0:3]	0x0	Brake by FET off duration: $N \times \text{BRAKE\_FET\_ON\_DURATION}$
				20:16	BRAKE_FREQUENCY_TOO_HIGH_TH	[0:31]	0x0	Brake frequency too high threshold: $(N+1) \times 3.125\%$ of maximum (system) speed
				23:21	BRAKE_FREQUENCY_TOO_HIGH_COAST_TIME	[0:7]	0x0	Brake frequency too high coast time: $2^{(N+1)}$ of system-timer interrupts
25:24	STRONG_ALGN_CURR_GAIN	[0:3]	0x0	Align current reference gain in brake in windmill condition: $N+1$				
31:26	BEMF_COMP_AMPLITUDE	[0:63]	0x0	Amplitude of compensating component: $N \times 0.390625\%$ of nominal voltage: 0 = disable BEMF compensator				
4D2	472	18	18	6:0	STPD_TH	[0:127]	0x0	Stopped threshold, below which this speed level, the rotor is considered stationary: $(N+1) \times 0.0244140625\%$ of maximum (system) speed
				9:7	PO_OPER	[0:7]	0x0	Position observer operational, below which speed, the position observer operates unreliably: $(N+1) \times 0.1953125\%$ of maximum (system) speed
				15:10	DEFAULT_EXT_CMD	[0:63]	0x0	Default external command value: $N \times 1.5625\%$ of maximum command
				21:16	CMD_ON_TH	[0:63]	0x0	Command on threshold: $(N+1) \times 0.390625\%$ of maximum command
				27:22	CMD_OFF_TH	[0:63]	0x0	Command off threshold: $N \times 0.390625\%$ of maximum command
				28	RESERVED	[0:1]	0x0	Reserved
				30:29	RESERVED	[0:3]	0x0	Reserved
31	SOFT_OFF_BRAKE_EN	[0:1]	0x0	Soft-off brake enable: 0 = disabled 1 = enabled				

I <sup>2</sup> C EEPROM NVM Register (Hex)	I <sup>2</sup> C Shadow Register (Hex)	EE Address (Hex)	NVM	Bits	Name	Value (Dec)	Default	Description
4D3	473	19	19	2:0	SFOC_DECEL_OL_SPEED_TH	[0:7]	0x0	Deceleration open-loop speed threshold: (N + 1) × 0.390625% of maximum (system) speed
				3	SOFT_OFF_EN	[0:1]	0x0	Soft-off enable: 0 = disabled 1 = enabled
				9:4	SOFT_OFF_FREQUENCY_TH	[0:63]	0x0	Soft-off frequency threshold: (N + 1) × 0.1953125% of maximum (system) speed
				11:10	PIN_DIR_D_EB	[0:3]	0x0	DIR pin debounce time 0 = 0 ns 1 = 840 ns 2 = 12.76 μs 3 = 127.6 μs
				13:12	PIN_NBRAKE_D_EB	[0:3]	0x0	nBRAKE pin debounce time: 0 = 0 ns 1 = 840 ns 2 = 12.76 μs 3 = 127.6 μs
				14	DEFAULT_NBRAKE	[0:1]	0x0	Default nBRAKE bit value (inverse): 0 = no brake 1 = brake
				19:15	SFOC_DECEL_RATE	[0:31]	0x0	Deceleration rate: 0.0244140625% of maximum (system) speed during (N + 1) × 32 VCL updates
				24:20	SFOC_DECEL_OL_D_CURR_REF	[0:31]	0x0	Deceleration open-loop D current reference: (N + 1) × 3.125% of maximum current
				29:25	RESERVED	[0:31]	0x0	Reserved
				30	SFOC_QUIET_START_EN	[0:1]	0x0	Enable quiet start: 0 = disabled 1 = enabled
31	SFOC_SOFT_START_EN	[0:1]	0x0	Enable soft start: 0 = disabled 1 = enabled				
4D4	474	20	20	6:0	OVVL_VOLT_TH	[0:127]	0x0	Overvoltage variable limiter voltage threshold: 7.21875 V + N × 1.03125 V
				14:7	OVVL_VAR_LMT	[0:255]	0x0	Overvoltage variable limiter, variable limit: (N + 1) × 0.390625% of maximum variable value
				15	OVVL_ENABLE	[0:1]	0x0	Overvoltage variable limiter enable: 0 = disabled 1 = enabled
				22:16	ROT_START_RETRY_TOUT	[0:127]	0x0	Rotor start retry timeout: N of system timer interrupts
				26:23	ROT_START_RETRY_MAX_ATTEMPTS	[0:15]	0x0	Rotor start retry maximum attempts: 0 = infinite number of attempts 1:15 = N attempts
				27	CLK_COMP_ENABLE	[0:1]	0x0	Clock-compensation feature enable
				31:28	CLK_COMP_REF	[0:15]	0x0	Clock-compensation carrier frequency: 0 = 88.9 Hz 1 = 133.3 Hz 2 = 177.7 Hz 3 = 222.2 Hz 4 = 266.7 Hz 5 = 311.1 Hz 6 = 355.5 Hz 7 = 400 Hz 8 = 444.4 Hz 9 = 488.9 Hz 10 = 533.3 Hz 11 = 577.8 Hz 12 = 622.2 Hz 13 = 666.7 Hz 14 = 711.1 Hz 15 = 888.9 Hz

I <sup>2</sup> C EEPROM NVM Register (Hex)	I <sup>2</sup> C Shadow Register (Hex)	EE Address (Hex)	NVM	Bits	Name	Value (Dec)	Default	Description
4D5	475	21	21	17:13	SFOCSTARTCURRLMT	[0:31]	0x0	Phase current limit at the transition to the closed-loop: $(N + 1) \times 3.125\%$ of maximum current
				20:18	SFOCSOFTSTARTTIME	[0:7]	0x0	Soft start time: $256 \times (N + 1)$ VCL updates
				23:21	SFOCQUIETSTARTTIME	[0:7]	0x0	Quiet start (OL → CL transition) duration: $512 \times (N + 1)$ VCL updates
				27:24	SFOCDRVCURRRATELMT	[0:15]	0x0	Current rate limit in drive mode: $[2^{(N+1)} \times 0.745 \mu\%]$ of maximum current per VCL update
				31:28	SFOCGENCURRRATELMT	[0:15]	0x0	Current rate limit in generator mode: $[2^{(N+1)} \times 0.745 \mu\%]$ of maximum current per VCL update
4D6	476	22	22	15:0	UCC_X0	[0:65535]	0x0	UCC: x point 0
				31:16	UCC_X1	[0:65535]	0x0	UCC: x point 1
4D7	477	23	23	15:0	UCC_X2	[0:65535]	0x0	UCC: x point 2
				31:16	UCC_X3	[0:65535]	0x0	UCC: x point 3
4D8	478	24	24	15:0	UCC_X4	[0:65535]	0x0	UCC: x point 4
				31:16	UCC_X5	[0:65535]	0x0	UCC: x point 5
4D9	479	25	25	15:0	UCC_X6	[0:65535]	0x0	UCC: x point 6
				31:16	UCC_X7	[0:65535]	0x0	UCC: x point 7
4DA	47A	26	26	15:0	UCC_X8	[0:65535]	0x0	UCC: x point 8
				31:16	UCC_X9	[0:65535]	0x0	UCC: x point 9
4DB	47B	27	27	15:0	UCC_Y0	[0:65535]	0x0	UCC: Y point 0
				31:16	UCC_Y1	[0:65535]	0x0	UCC: Y point 1
4DC	47C	28	28	15:0	UCC_Y2	[0:65535]	0x0	UCC: Y point 2
				31:16	UCC_Y3	[0:65535]	0x0	UCC: Y point 3
4DD	47D	29	29	15:0	UCC_Y4	[0:65535]	0x0	UCC: Y point 4
				31:16	UCC_Y5	[0:65535]	0x0	UCC: Y point 5
4DE	47E	30	30	15:0	UCC_Y6	[0:65535]	0x0	UCC: Y point 6
				31:16	UCC_Y7	[0:65535]	0x0	UCC: Y point 7
4DF	47F	31	31	15:0	UCC_Y8	[0:65535]	0x0	UCC: Y point 8
				31:16	UCC_Y9	[0:65535]	0x0	UCC: Y point 9

**USER REGISTERS**

Registers not shown are not for user access. Any change to a value in the undocumented registers may cause a malfunction or damage to the part.

I <sup>2</sup> C Address (Hex)	Field Name	Bits	Read/Write [1]	Default Value	Description
0x0	REG: SW_STATUS	31:0	RO	0x0	Refer to the SW Status Register, SW_STATUS section
0x1	REG: REF_CMD	16:0	RW	0x0	Refer to the I <sup>2</sup> C Command Register, REF_CMD section
0x2	REG: BRAKE_CTRL	0:0	RW	0x0	0 = brake is applied (via register or via nBRAKE pin) 1 = brake is not applied

[1] RO = Read-Only; RW = Read/Write

## SW Status Register, SW\_STATUS

The software status read-only register at address (0x0000) contains the motor control mode, state, fault, and status flags.

Address 0x0000, Read-Only				
Variable Name	Bits	Size	Type	Description
<b>Controller Mode</b>				
MCA_MODE	7:0	8 bits	MC_MODE_T	Motor control mode OFF_MC_MODE STANDBY_MC_MODE ROTATE_MC_MODE BRAKE_MC_MODE FAIL_MC_MODE DEBUG_MC_MODE
<b>Controller State</b>				
MCA_FSMSTATE	15:8	8 bits	MC_FSMSTATE_T	Motor control FSM state IDLE_MC_FSMSTATE SBY_MC_FSMSTATE WNDML_MC_FSMSTATE BRAKE_MC_FSMSTATE FAIL_MC_FSMSTATE IPDORALIGN_MC_FSMSTATE RAMPUP_MC_FSMSTATE DRIVE_MC_FSMSTATE
<b>Fault Status</b>				
OV	16	1 bit	fault/status flag	Over voltage
UV	17	1 bit	fault/status flag	Under voltage
OT	18	1 bit	fault/status flag	Over temperature
OC	19	1 bit	fault/status flag	Over current latch
EE	20	1 bit	fault/status flag	EEPROM error
RS	21	1 bit	fault/status flag	Rotor stalled latch
NMS	22	1 bit	fault/status flag	No-motor start detection
OK	23	1 bit	fault/status flag	System OK
<b>Motor Control Status</b>				
VQ_LIM	24	1 bit	fault/status flag	V <sub>q</sub> limit
VD_LIM	25	1 bit	fault/status flag	V <sub>d</sub> limit
SPD_LIM	26	1 bit	fault/status flag	Speed limit
PWR_LIM	27	1 bit	fault/status flag	Power limit
VGEN_LIM	28	1 bit	fault/status flag	Voltage (generator mode) limit
OVV_LIM	29	1 bit	fault/status flag	Over voltage variable limit
ROT_SYNC	30	1 bit	fault/status flag	Rotor synchronized
[Reserved (zero)]	31	1 bit	zero	Reserved—reads as zero

**I<sup>2</sup>C Command Register, REF\_CMD**

This register is used with the I<sup>2</sup>C external command source to set the demand value and to control the motor direction.

I <sup>2</sup> C Address (Hex)	Bits	Value	Name	Description
0001	15:0	[0 ... 32767]	demand	Sets the speed control demand
	16	[0 ... 1]	direction	Sets the motor spin direction

## SW FIXED-ADDRESS VARIABLES

With I<sup>2</sup>C, it is possible to access status variables that reside at fixed addresses. Addresses of these variables, their types, and sizes are provided in the table that follows.

Variable Name	Address	Size	Type	Description
MPCI_VALUE	0x0385	4B	UINT32_T	Interface variable of multi-purpose control interface (MPCI): Bits [15:0] = Data written into MPCI Bits [32:16] = MPCI Instruction (code of functionality to execute)
MCA_THETA	0x0386 [LSB, 15:0]	2B	INT16	Start rotor position, 9-bit resolution (0.3515625° per bit): -512 (sign extended to 16 bits) = -180° 511 = 179.99° 0 = 0°
MCA_FREQ	0x0386 [MSB, 31:16]	2B	INT16	Start rotor frequency, SFOC_FREQ_RES (NVM parameter) resolution, sign represents rotation direction: Negative = Clockwise Positive = Counterclockwise Zero = Stationary
MCA_COMMAND	0x0387 [LSB, 15:0]	2B	INT16	Current value of command after UCC; 15-bit resolution, signed: -32768 = Maximum negative command (-100%) 32767 = Maximum positive command (99.99%) 0 = 0 command (0%)
IPD_ERRSTATUS	0x0387 [bit position, 23:26]	1B	IPD_ERRSTATUS_T	IPD execution status: 0 = OK (IPD finished successfully) 1 = STG1_ERROR_INDUCT_EQUAL_IPD 2 = STG2_ERROR_TIMEOUT_IPD 3 = STG2_ERROR_EQUAL_SATURATION_IPD
WNDML_ERRSTATUS	0x0387 [MSB, 31:24]	1B	WNDMLERRSTATUS_T	Windmill execution status: 0 = OK (windmill completed successfully) ERR_BEMF_SEQUENCE_WNDML ERR_BEMF_VALUE_WNDML
MCA_EXTCMD	0x0388 [LSB, 15:0]	2B	UINT16	Input of the curve transformer
V_BUS	0x038A [LSB, 15:0]	2B	UINT16	V <sub>BB</sub> voltage: $V_{BB} = (\text{value}) \times [(2 \times 1.2/4096) \times 40]$ [V]
V_CMD	0x038A [MSB, 31:16]	2B	UINT16	Voltage command, 12-bit resolution
I_BUS	0x038B [LSB, 15:0]	2B	INT16	I <sub>BB</sub> current, signed: $I_{BB} = 1.5 \times (\text{value}/2048) \times (0.57735) \times \text{maximum current}$ [A]
FG_FREQ	0x038C	4B	INT32	FG frequency, SFOC_FREQ_RES resolution, sign represents rotation direction: Negative = Clockwise Positive = Counterclockwise Zero = Stationary
VBEMF	0x038D [LSB, 15:0]	2B	INT16	Back-EMF voltage (available in position-observer closed-loop mode of operation), signed: $V_{BEMF} = (\text{value}/16384) \times (0.57735) \times (\text{nominal voltage, V})$ [V]

## FOC INTERNAL VARIABLES

Variable Name	Address	Size	Type	Description
THETA_EST	0x04A1	4B	INT32	Start rotor position, 9-bit resolution (0.3515625° per bit): -512 (sign extended to 32 bits) = -180° 511 = 179.99° 0 = 0°
FREQ_EST	0x04A0	4B	INT32	Current rotor frequency, SFOC_FREQ_RES resolution, sign represents rotation direction: Negative = Clockwise Positive = Counterclockwise Zero = Stationary
ID	0x04A2	4B	INT32	D-axis current, signed: $I_D = (\text{value}/2048) \times \text{maximum current [A]}$
IQ	0x04A3	4B	INT32	Q-axis current, signed: $I_q = (\text{value}/2048) \times \text{maximum current [A]}$
VD	0x04A4	4B	INT32	D-axis voltage, signed: $V_d = (\text{value}/16384) \times (0.57735) \times (\text{nominal voltage, V}) [V]$
VQ	0x04A5	4B	INT32	Q-axis voltage, signed: $V_q = (\text{value}/16384) \times (0.57735) \times (\text{nominal voltage, V}) [V]$
HSD	0x04B1	4B	INT32	D-axis duty cycle, signed: $HS_d = (\text{value}) / \{(\text{PWM period, in clock periods}) \times [1 + (\text{PWM high-resolution mode, 0/1 if disabled/enabled})] \times (0.57735)\}$ , in parts
HSQ	0x04B2	4B	INT32	Q-axis duty cycle, signed: $HS_q = (\text{value}) / \{(\text{PWM period, in clock periods}) \times [1 + (\text{PWM High Resolution mode, 0/1 if disabled/enabled})] \times (0.57735)\}$ , in parts

## PROGRAMMING THE EEPROM

The NVM is read and written using the I<sup>2</sup>C interface.

### I<sup>2</sup>C SERIAL INTERFACE

The A89333-1 uses a standard fast-mode I<sup>2</sup>C serial port format to program the EEPROM or to control the IC operation serially. With the help of the GUI, the user can adjust configuration register values for a particular application before programming these parameters into EEPROM. The A89333-1 7-bit peripheral address is 0x55.

The I<sup>2</sup>C interface shares pins with PWM/SPD or FG/RD. The PWM/SPD pin functions as the clock (SCL) input, and the FG/RD pin is the data line (SDA). A special sequence is not needed to begin transferring data. If the motor is running, the FG may pull the data line low while trying to initialize in serial port mode. Once an I<sup>2</sup>C command is sent, the PWM input is ignored. For more information, refer to the VBB, UV, and NVM Reprogramming section.

Because RD is typically low when faults are not present, if the FG/RD option is set to RD, the establishment of an I<sup>2</sup>C communication requires the RD pull-down to be disabled by reducing V<sub>BB</sub> to less than V<sub>BBUVLO</sub>. For more information, refer to the VBB, UV, and NVM Reprogramming section.

### I<sup>2</sup>C Timing Diagrams

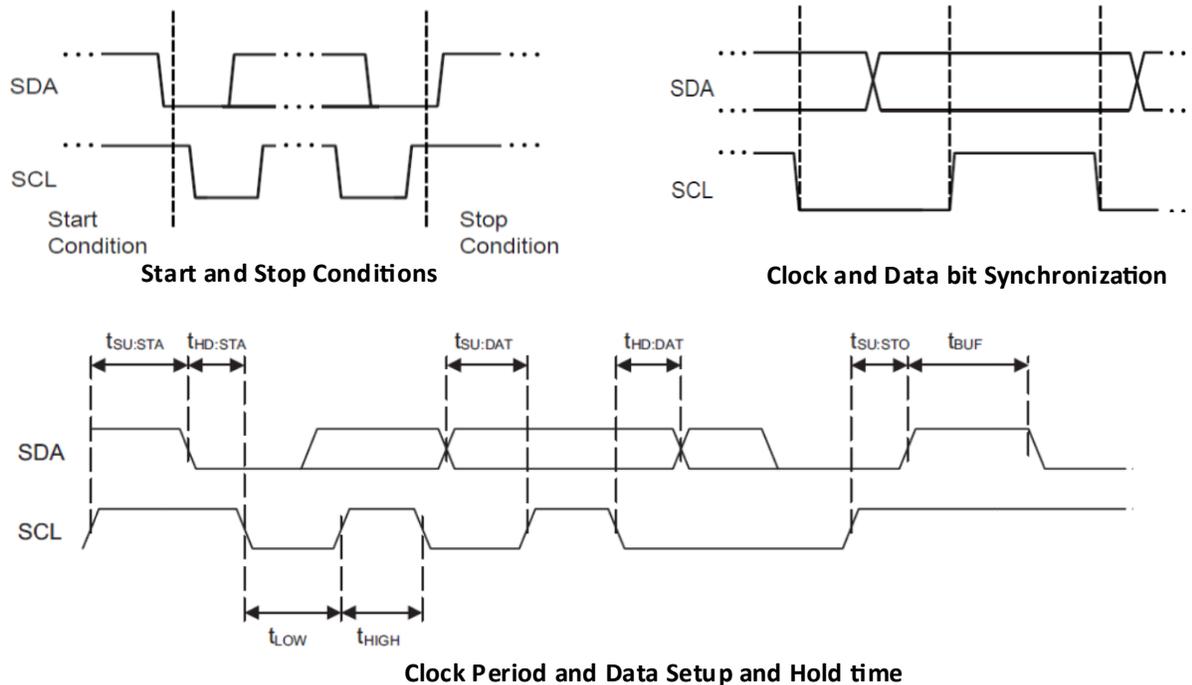


Figure 20: I<sup>2</sup>C-Compatible Timing Requirements

### READ PROCEDURE

1. Start condition

2. (1 byte) 7-bit I<sup>2</sup>C peripheral address (device ID) 1010101, R/W bit = 1
3. (1 byte) Fixed bit = 1, bits [6:0] of the internal register address
4. (1 byte) Fixed bit = 1, bits [13:7] of the internal register address
5. (4 bytes) read four data bytes, least significant byte first, the last byte should be NACK'd by the controller
6. Stop condition

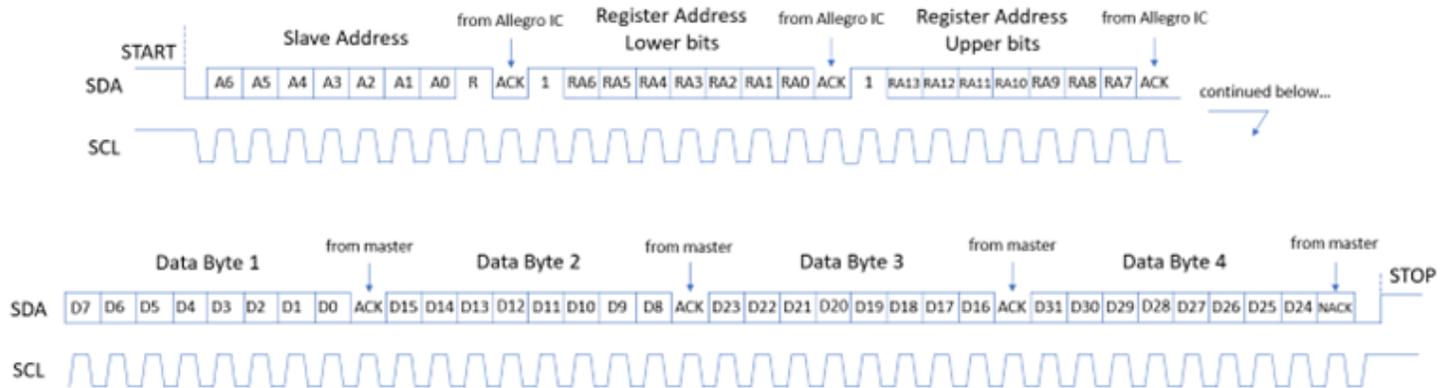


Figure 21: Read Procedure

## WRITE PROCEDURE

1. Start condition
2. (1 byte) 7-bit I<sup>2</sup>C peripheral address (device ID) 1010101, R/W Bit = 0
3. (1 byte) Fixed bit = 1, bits [6:0] of the internal register address
4. (1 byte) Fixed bit = 1, bits [13:7] of the internal register address
5. (4 bytes) four data bytes, least significant byte first
6. Stop condition

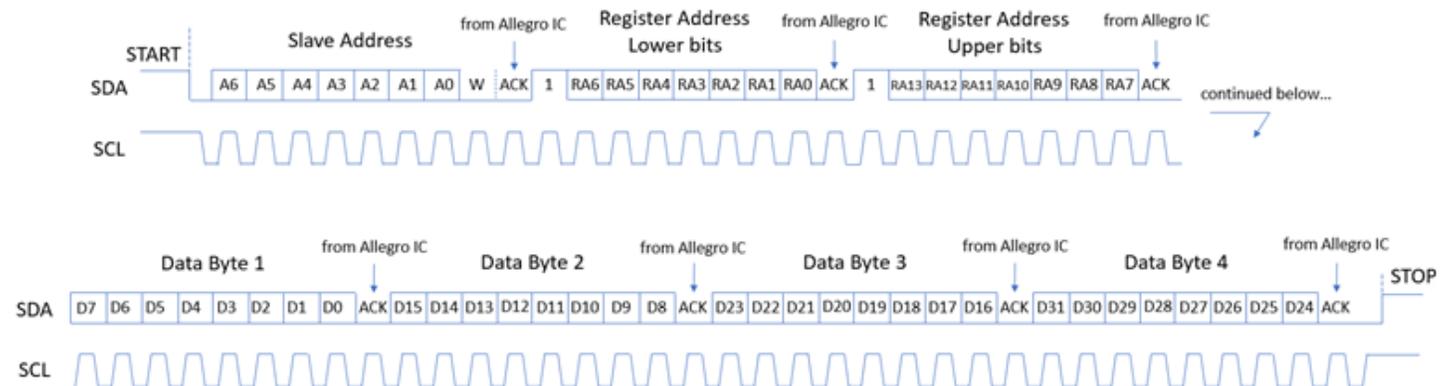


Figure 22: Write Procedure

## Operation Modes and Customer Password Protection

A89333-1 implements customer password protection of I<sup>2</sup>C access to certain regions of memory space—foremost, the copy of customer settings in shadow registers.

The A89333-1 operation modes are:

Name	Description
Application Mode (AM)	I <sup>2</sup> C has access to user registers and fixed-address variables Default mode after power up
User Mode (UM)	I <sup>2</sup> C has access to user registers, fixed-address variables, FOC internal variables, shadow registers, and NVM EEPROM configuration registers

The password length is 16 bits, and the password is set by the customer by configuring the corresponding parameter (CUSTOMER\_PASSWORD) in the NVM. (Alternatively, the password can be set by Allegro, upon first-part configuration.)

All combinations other than 0x0000 and 0xFFFF are considered valid passwords.

If a password combination is set to 0x0000 or 0xFFFF, the customer password is not configured and the part enters user mode after POR. In this way, when the part arrives, the customer has access to NVM EEPROM to set the user mode password (by configuring the corresponding parameter, CUSTOMER\_PASSWORD, in NVM). Once the user mode password is configured, the part enters application mode after POR and the EEPROM NVM and shadow registers are protected.

To change the operation mode, write to the MPC\_I\_VALUE\_GLOBAL variable via the I<sup>2</sup>C 32-bit frame. The variable (MPC\_I\_VALUE\_GLOBAL) consists of two parts, each 16 bits wide:

1. Instruction code is contained in the MSBs [31:16]; the instruction code for the customer password check is 0x01.
2. Data (i.e., password combination) is contained in the LSBs [15:0].

Functionality	Instruction Code	Example of Transaction Content Value [1]	Execution
Customer Password Check	0x01	Bits [31:16] = 0x01, instruction code Bits [15:0], password to be entered	The device acknowledges Customer password entry by rewriting Instruction code and Data (bits [31:0]) with zero (0x00) and performs password check.  Customer password entry and check can be executed in any state of the motor controller.

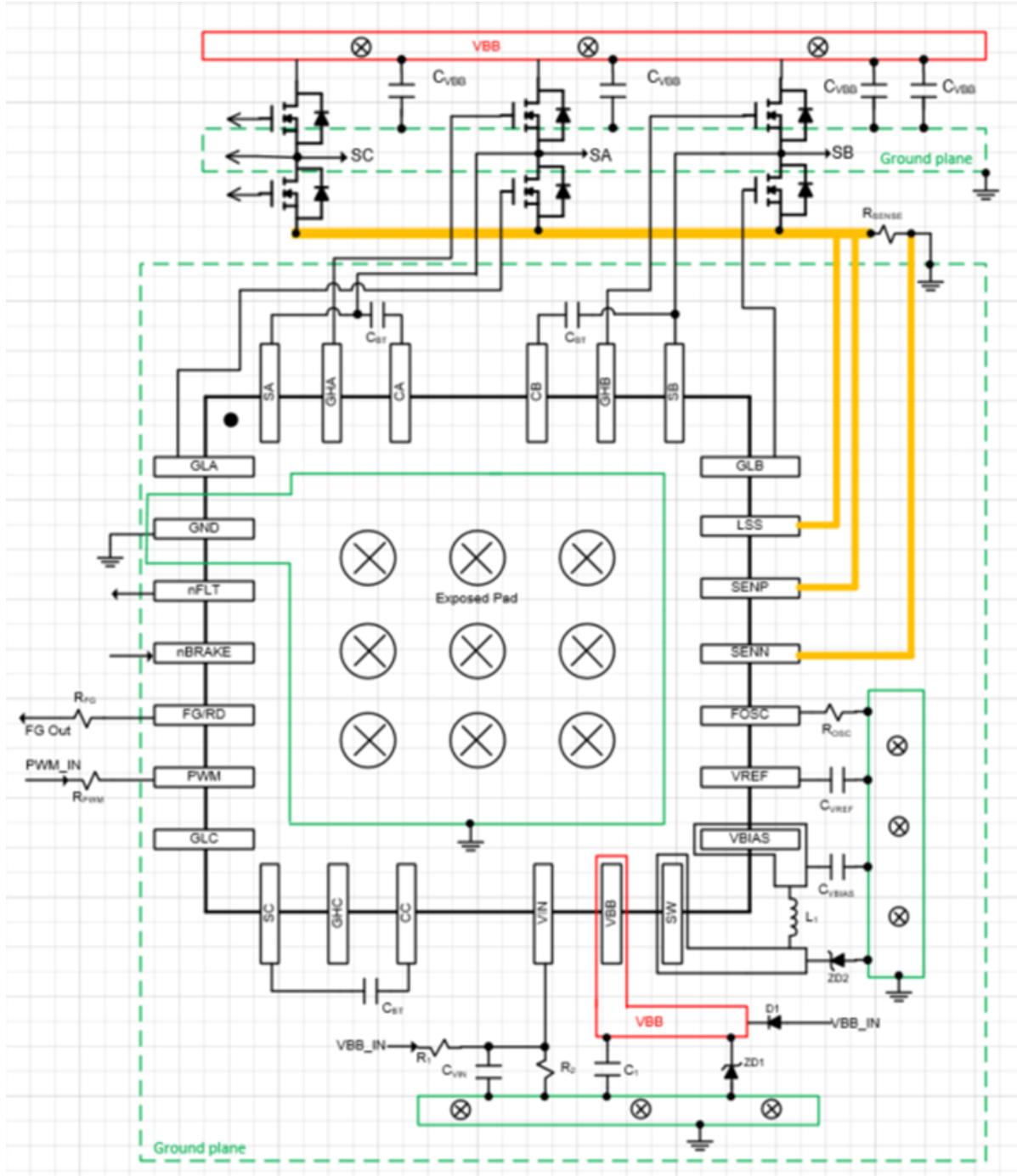
[1] This is the value written into the MPC\_I\_VALUE\_GLOBAL variable via the I<sup>2</sup>C 32-bit frame.

If a valid customer password is configured, the controller remains in the application operation mode, where user registers and fixed-address variables can be accessed, until the configured password is correctly entered with MPC\_I\_VALUE\_GLOBAL.

Once the password is entered correctly, the controller enters the user operation mode and the following configuration registers can be accessed: user registers, fixed-address variables, FOC internal variables, shadow registers, and NVM EEPROM.

If an incorrect combination is entered three times in a row using MPC\_I\_VALUE\_GLOBAL, the controller must be rebooted (by POR) before further checks of the customer password can be performed.

APPLICATION INFORMATION

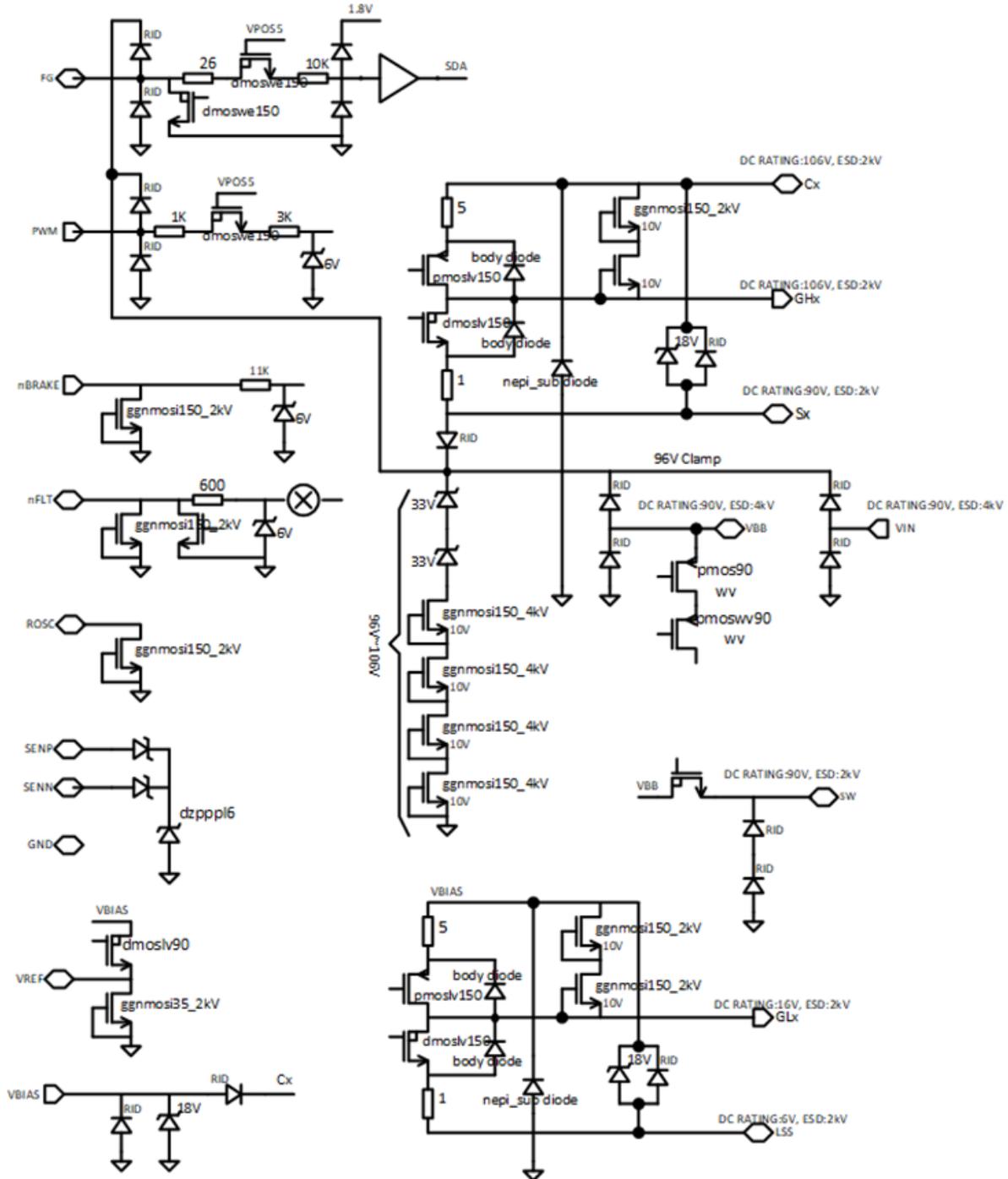


Name	Suggested	Comment
C <sub>VREF</sub>	4.7 $\mu$ F/X5R/10 V	Ceramic capacitor required
C <sub>VBB</sub>	10 $\mu$ F – 47 $\mu$ F/50 V	Power-supply stabilization; electrolytic or ceramic OK
R <sub>PU</sub> , R <sub>FGPU</sub>	10 k $\Omega$	Pull-up resistors to VREF
C <sub>BT</sub>	0.22 $\mu$ F/25 V	Bootstrap capacitor, ceramic capacitor required
C <sub>VBIAS</sub>	10 $\mu$ F/50 V	Ceramic capacitor required
C1	0.1 – 0.47 $\mu$ F/50 V	Ceramic capacitor required
D1	HSM8100JE3/TR13	Required to isolate motor for reverse-polarity protection
ZD1 (optional)	SMBJ40A	TVS to limit maximum V <sub>BB</sub> due to transients due to motor generation on power line
L1	10 $\mu$ H (994-PFL4514-103MEC)	Higher value of inductor can also be used; ensure inductor is not saturated
ZD2	SDM1100LP-7	Schottky diode required; ensure current rating is high enough to handle the inductor current
R <sub>FG</sub> , R <sub>PWM</sub>	500 $\Omega$	Isolate IC pins from noise or overvoltage transients or protect from connector issues
R <sub>OSC</sub>	25 k $\Omega$ $\pm$ 0.1%	Required for better oscillator accuracy
R <sub>sense</sub>	100 m $\Omega$ $\pm$ 1%	Current sense resistor and value depends on the maximum current of the system
R1	10 k $\Omega$	Required for reverse polarity protection VIN pin
R2	10 k $\Omega$	Pull-down for VIN
C <sub>VIN</sub>	0.1 $\mu$ F	Noise filter for hot-swap events

## LAYOUT NOTES

1. Add thermal vias to exposed pad area.
2. Add ground plane on top and bottom of PCB.
3. Place R<sub>sense</sub> close to the bridge and use Kelvin sensing.
4. Place C<sub>VREF</sub> and C1 as close as practical to the IC, connected to the GND plane.
5. Place L1, ZD2 and C<sub>VBIAS</sub> as close as practical to the IC, connected to the GND plane.
6. Place C<sub>BT</sub> as close as practical to the IC.
7. Place C<sub>VBB</sub> close to the V<sub>BB</sub> power rail of the external FETs.

## PIN DIAGRAM



## PACKAGE OUTLINE DRAWING For Reference Only – Not for Tooling Use

(Reference Allegro DWG-0000222, Rev. 4)  
NOT TO SCALE

All dimensions nominal unless otherwise stated – Dimensions in millimeters  
Exact case and lead configuration at supplier discretion within limits shown

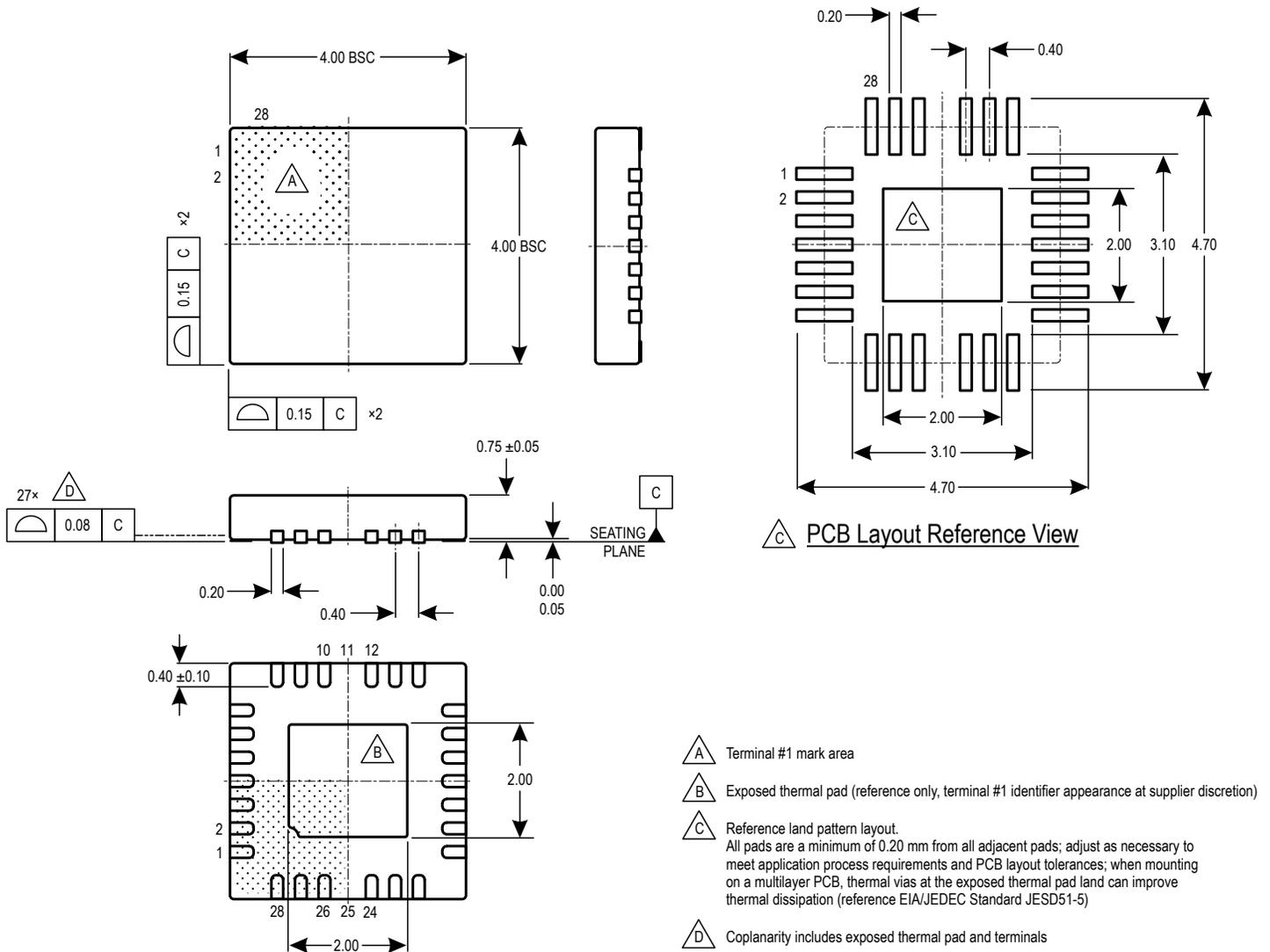


Figure 23: EC Package, 28-Pin QFN with Exposed Pad

## Revision History

Number	Date	Description
–	March 26, 2025	Initial release

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